

Parasitic Effects from Cooling of GaN Power Transistors - Impact on Switching Losses

Pelle Weiler, Bart Bokmans, Erik Lemmen, Bas Vermulst, Korneel Wijnands

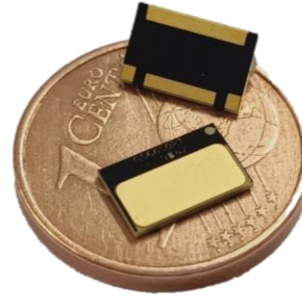
Gallium-Nitride FETs

GaN is becoming a very attractive choice for applications with volume or efficiency restrictions

Benefits

Small size → high power density

High dV/dt → low switching energy



GaN Systems GS66508T

- 650 V 50 mΩ
- Bottom Side: Drain, Gate, Source
- Top Side: Cooling Pad (Source)

Challenges

Small size → little cooling area

High dv/dt → possible EMI issues

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Agenda

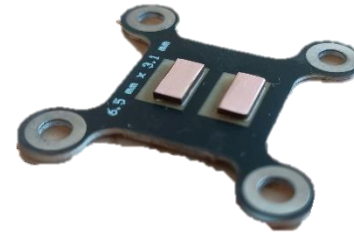
Cooling Solution for GaN devices

- IMS heat-spreaders
- Material limits

Experimental Verification

- Double pulse setup
- High-bandwidth shunt
- Switching Waveforms
- Switching Losses

Conclusion

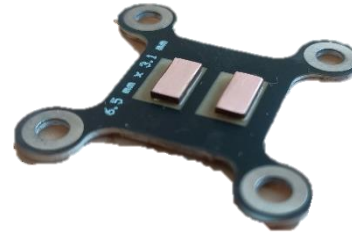


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IMS Heat-Spreaders

Insulated Metal Substrates

- Aluminium base laminated with insulating polymer and copper
- Ordered same as regular PCB
- Easy custom solutions for non-standard GaN packages



IMS Heat-Spreaders

Copper Layer

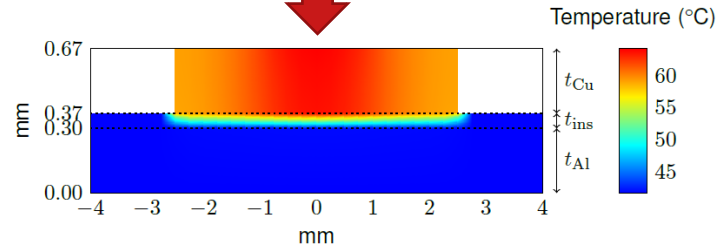
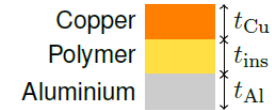
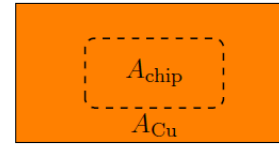
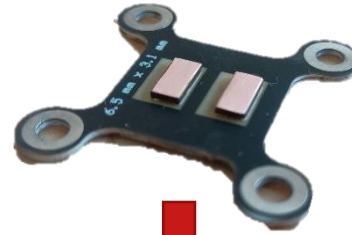
- High thermal conductivity (380 W/m/K)
- Spreads the heat horizontally
- Requires sufficient thickness ($> 300 \mu\text{m}$)

Insulation Layer

- Low thermal conductivity (1-10 W/m/K)
- As thin as possible ($< 100 \mu\text{m}$)
- Limits thermal path
- Adds parasitic capacitance

Aluminium Layer

- Structural support (1-1.5 mm)
- Mounted against heat-sink



Source: Design Limitations of heat spreaders for gallium-nitride power modules, P. Weiler, PCIM 2020

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IMS Heat-Spreaders

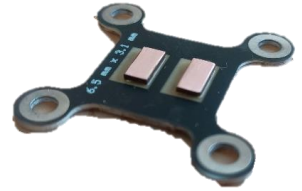
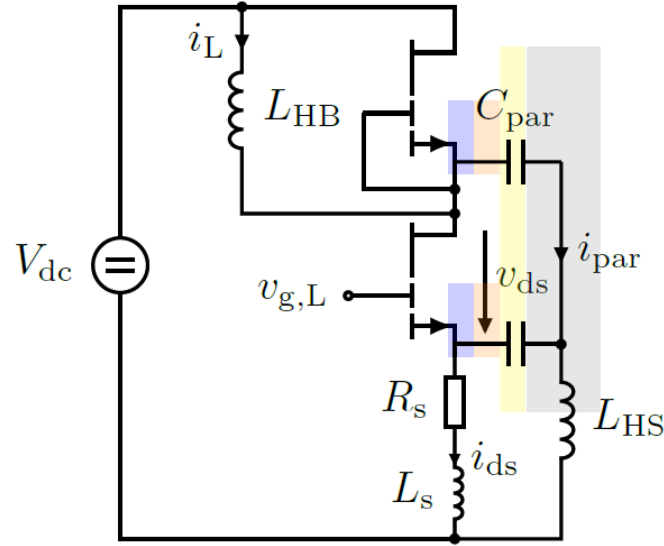
Parasitic capacitance

- Connected from switching node to heatsink
- High dv/dt induces current
- Linked to thermal resistance

$$R_{th,ins} = \frac{1}{\kappa_{ins}} \frac{A_{Cu}}{d_{ins}}$$

$$C_{par} = \varepsilon_0 \varepsilon_r \frac{d_{ins}}{A_{Cu}}$$

$$C_{par} = \frac{\varepsilon_0 \varepsilon_r}{\kappa_{ins} R_{th,ins}}$$



Material	κ [$\frac{W}{mK}$]	ε_r	$\frac{\kappa}{\varepsilon_0 \varepsilon_r}$ [$\frac{W}{pFK}$]
FR4	0.25	4.5	0.006
VT-4B3	3	4.8	0.07
VT-4B7	7	4.8	0.17
Al2O3	20	9	0.25
AlN	180	9	2.26

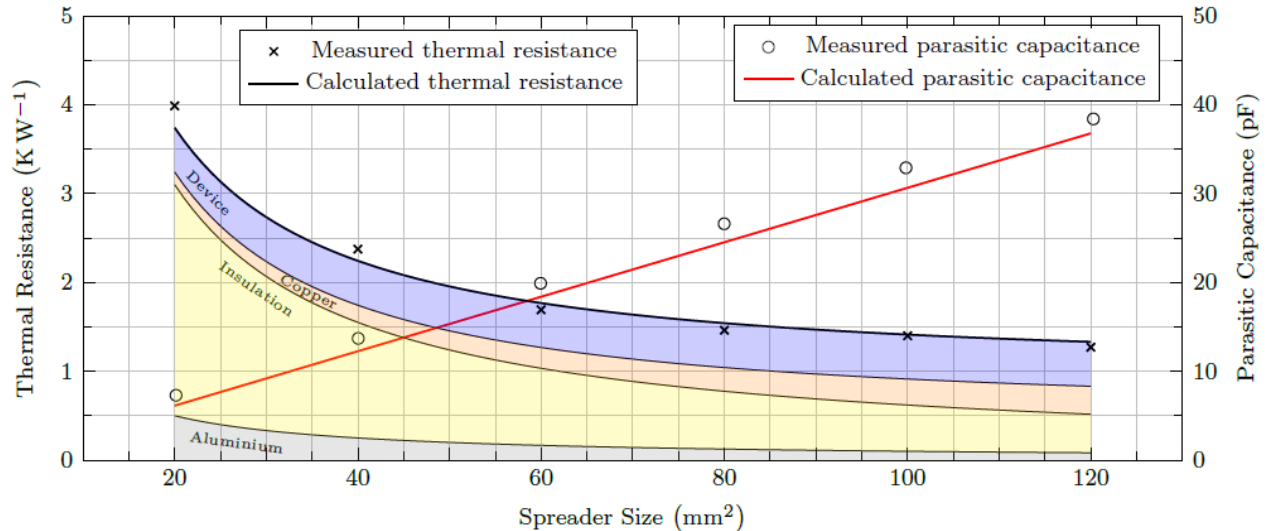
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IMS Heat-Spreaders

Range of heat-spreaders

- 1-6 x chip area
- Low conductive
 - $\kappa_{\text{ins}} = 1 \text{ W/m/K}$
- Low capacitive
 - $\epsilon_r = 1.8$
- 1 mm thick copper

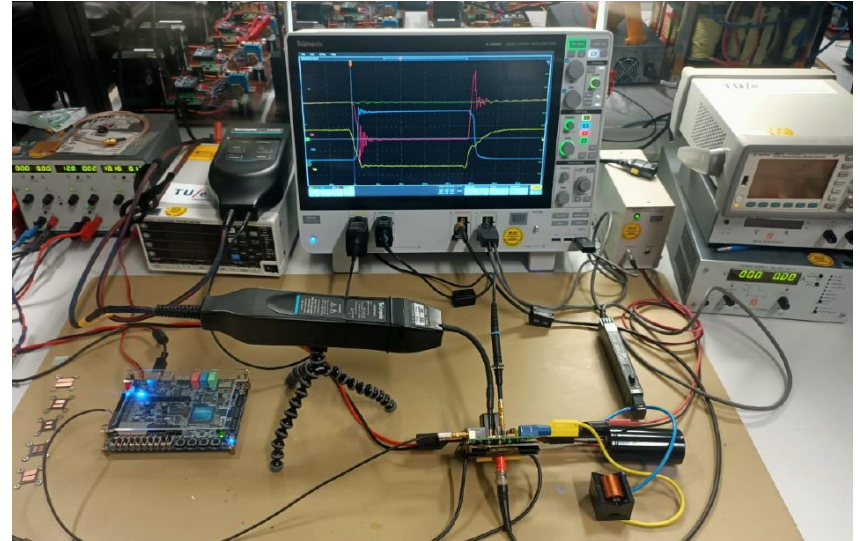
→ Investigate effect on switching performance



Experimental Verification

Double Pulse Setup

- 400 V GaN half-bridge
- Calculate switching losses from device voltage and current
- Requires high bandwidth current measurement
 - Coaxial current shunt

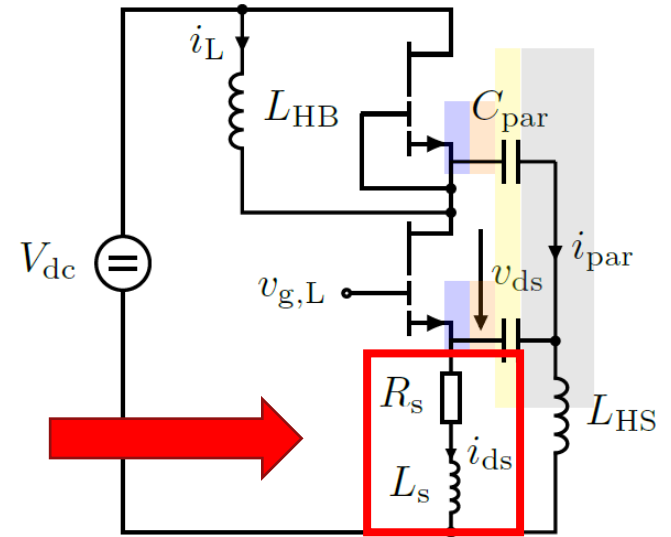


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Experimental Verification

Coaxial Current Shunt

- Passband up to 2 GHz
- 100 mΩ resistance
- Parasitic insertion inductance
 - Dependent on connection
 - In series to power loop inductance

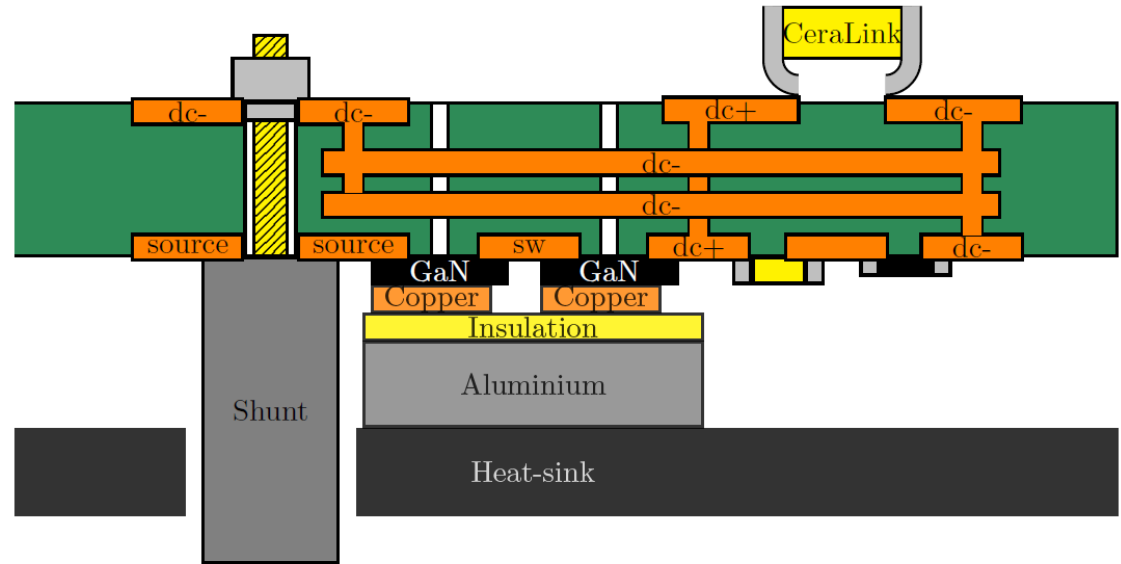


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Experimental Verification

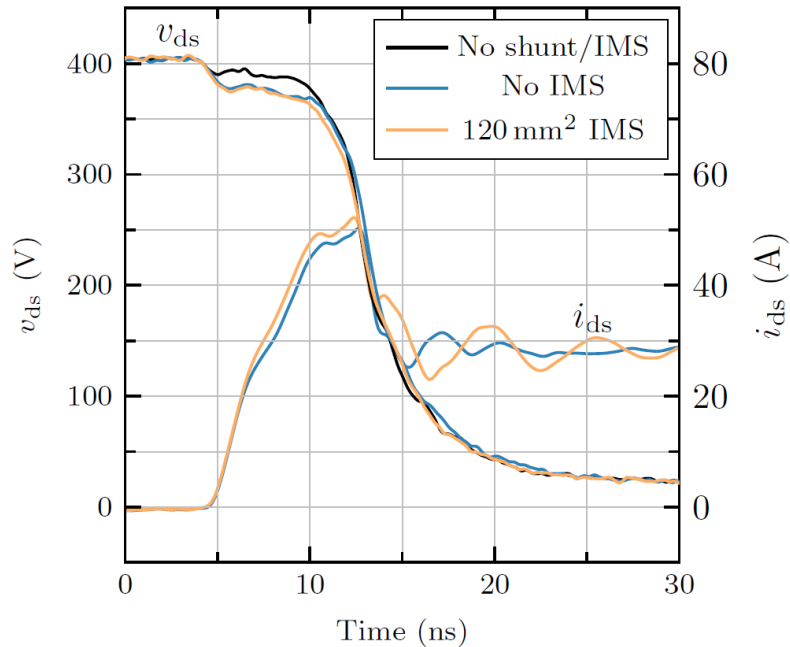
Board Design

- Shunt connected with M4 threaded insert
- dc- returned through internal layers for low loop inductance
- GaN devices connected to heat-spreader and heatsink
- RC snubber next to devices
- dc-link capacitor on top



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Experimental Verification

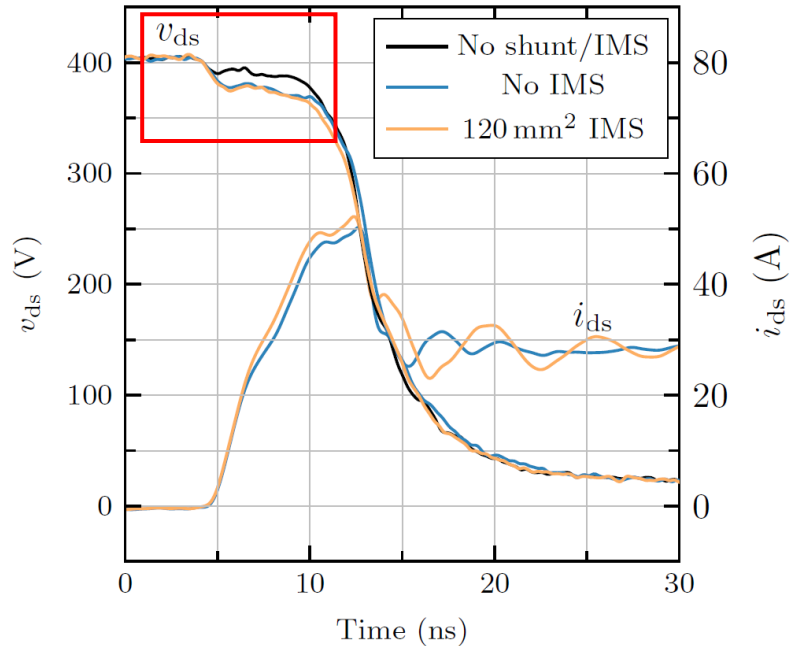


Turn-on

- Shunt has noticeable effect on initial voltage drop
 - Loop inductance resists commutation
- No cooling
 - Lower peak current
 - Less ringing
- 120 mm² IMS
 - Increased peak current
 - More ringing

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Experimental Verification

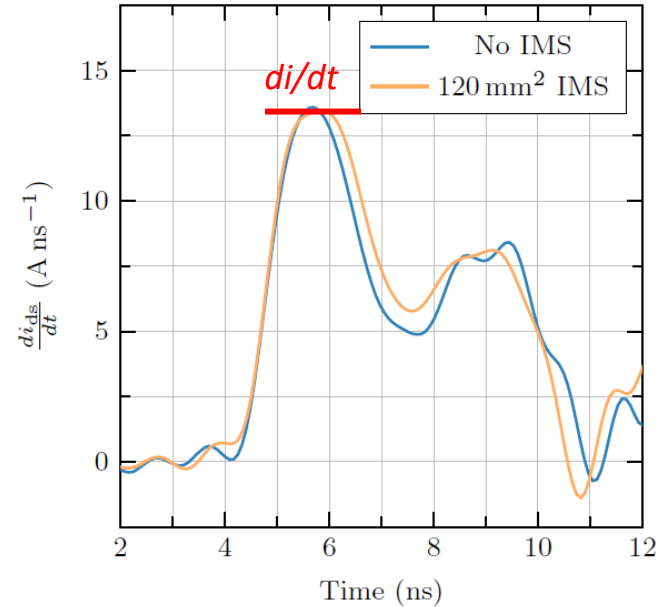
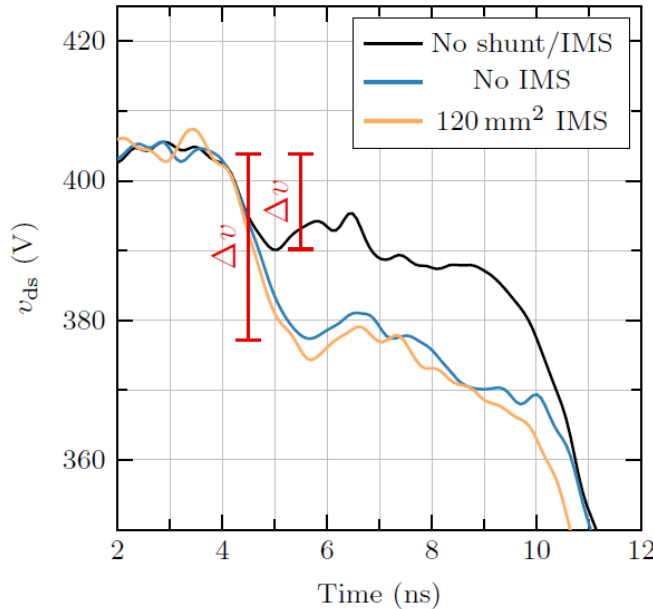


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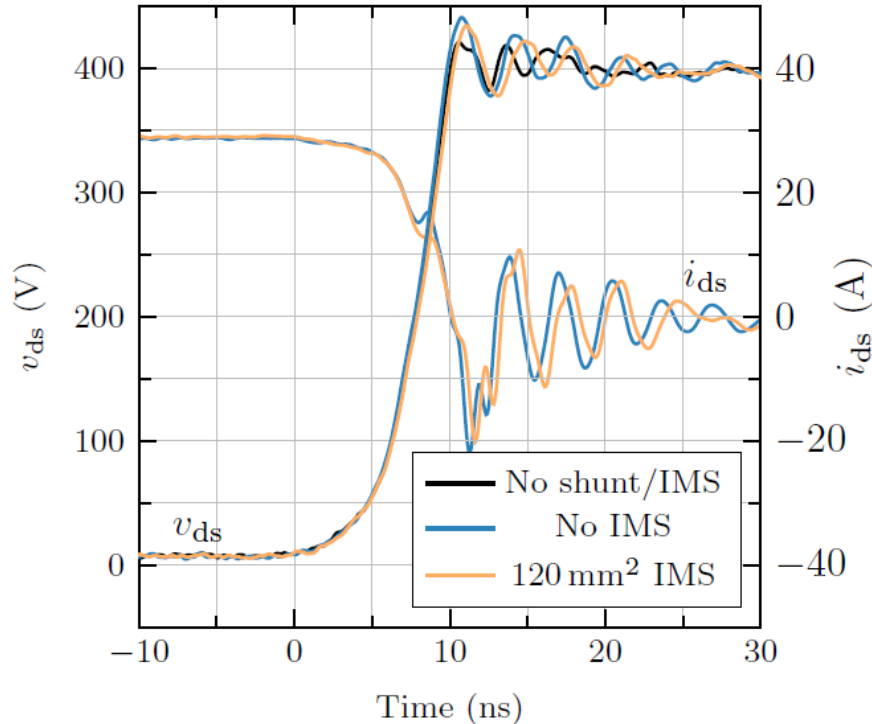
Experimental Verification



Turn-on

- Voltage drop proportional to loop inductance and di/dt
→ Estimated insertion inductance of shunt ~ 1 nH

Experimental Verification

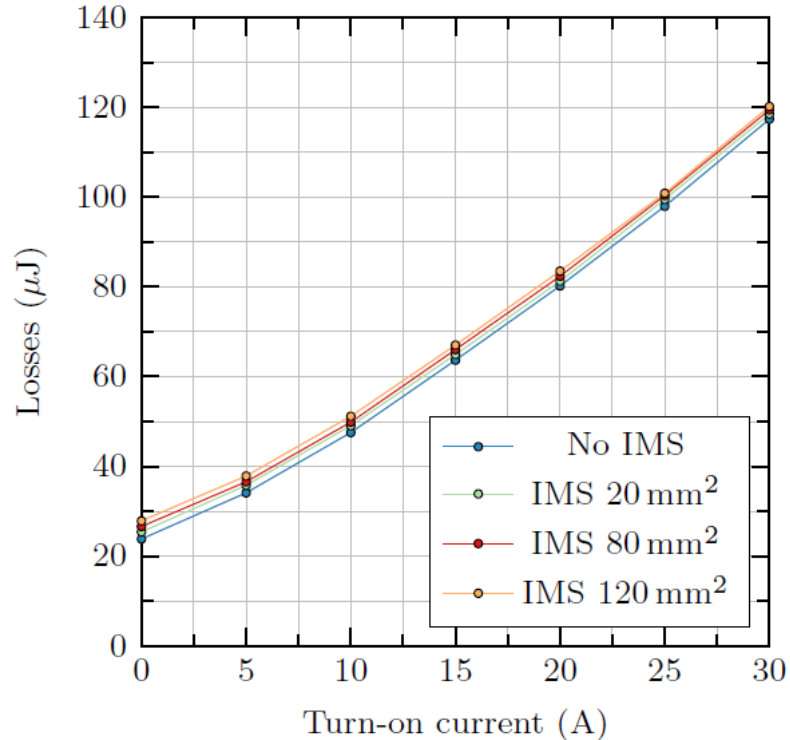


Turn-off

- Shunt insertion inductance causes larger overshoot
- Little perceivable difference between no cooling and 120 mm² IMS

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Experimental Verification



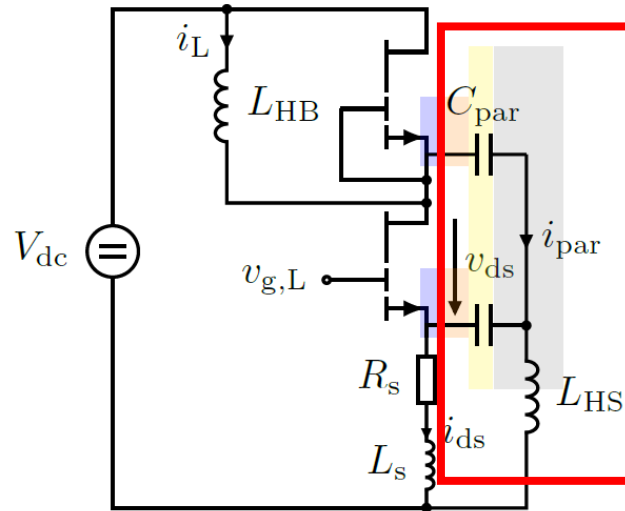
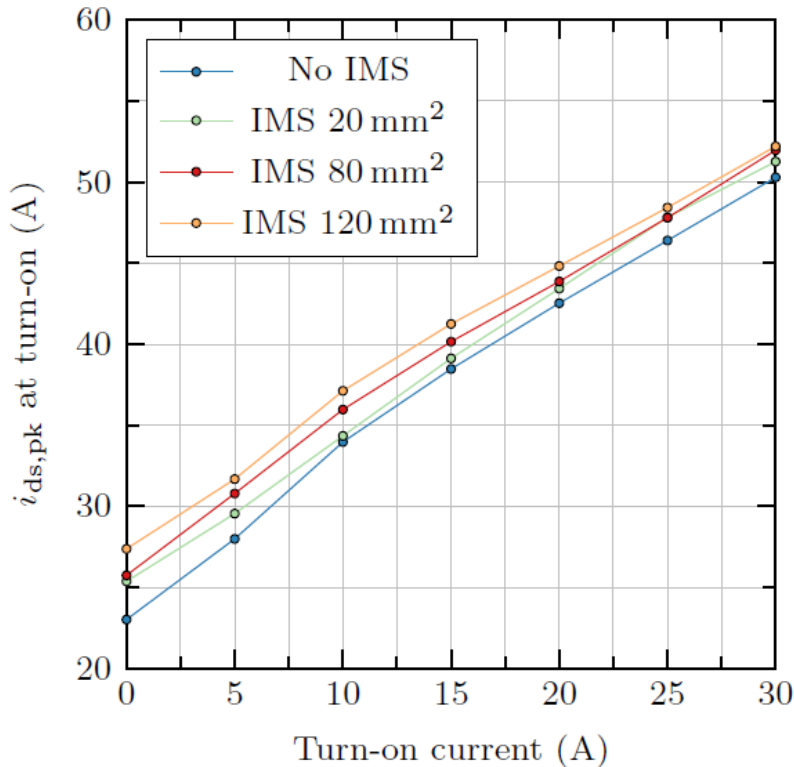
Switching Losses

- Increase in losses of up to 4-5 μJ
 - 10% relative increase at 10 A
 - Absolute increase in losses is small

However, increased losses come from increased peak current

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Experimental Verification



Peak current

- Increased by parasitic heatspreader capacitance
- Up to 4 A
- Difference between no IMS and flows through heatsink

→ Potential EMI source

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Conclusion

Any form of cooling will alter the switching losses of GaN

Parasitic capacitance to heatsink must be included in characterization

- Noticeable impact from 40 pF
- Increased peak current

Excess induced current returns through heatsink

- Source for EMI

Lower capacitance comes at the cost of larger thermal resistance (using same material)

- Dictated by geometry
- Material coefficient $\kappa_{\text{ins}}/(\epsilon_0 \epsilon_r)$ determines best case performance for a given material



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Conclusion

IMS heat-spreaders

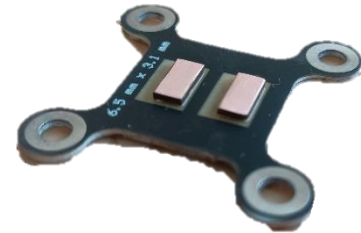
Customizable cooling solution for non-standard packages

Low dielectric constant reduces parasitic impact ($\epsilon_r = 1.8$)

→ Usually implies lower thermal resistance

Caution with high dielectric constants ($\epsilon_r > 4.5$)

→ Small areas can already lead to significant parasitic impact



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