

A New Modulation Method based on Switching Losses Minimization for DC-AC Inverters

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- Multilevel DC-AC inverters
- Preliminaries
- Proposed modulation method
- Simulation results
- Conclusion





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Multilevel DC-AC inverter

Many *applications*:

- photovoltaic systems
- high-voltage power transmissions
- electric motor drives

Characteristics:

- Controlled AC voltage source
 - \circ composed of >2 levels
 - \circ drives desired load currents







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Three-level NPC inverter

- Applications of few MW and kV
- Phase voltages $v_x = \{-v_{dc,l}, v_n, v_{dc,u}\}$
- 27 switch positions $u_{abc} = \{-1,0,1\}^3$
- *Clarke* transformation:

$$v_{\alpha\beta} = Pv_{abc}$$
, where $P = \frac{2}{3} \begin{bmatrix} 1 & -\frac{1}{2} & -\frac{1}{2} \\ 0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \end{bmatrix}$

 $v_{\rm dc,u}$

 $v_{\rm dc,l}$



Load current control schemes



Trade-off switching losses and THD

- Direct control: *trade-off*
- Indirect control: so far *performance* and *constraint* satisfaction
 - Trade-off done by modulator \rightarrow focus of this presentation
- Modulators (implicit trade-off):
 - *Soft switching type* modulation (switches around zero currents)
 - Discontinuous PWM (reduces number of switchings)
 - Space vector modulation (small voltage jumps)

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Three-level NPC inverter

- Switching *constraints*
 - Not directly between -1 and 1
 - In max 2 phase, in opposite inverter halves
- Neutral-point voltage balancing





Space vector modulation

- The *closest* triangle with v_1, v_2, v_3
- For every modulation cycle T_s : $t_1v_{1,\alpha} + t_2v_{2,\alpha} + t_3v_{3,\alpha} = T_sv_{\alpha}^*$ $t_1v_{1,\beta} + t_2v_{2,\beta} + t_3v_{3,\beta} = T_sv_{\beta}^*$ $t_1 + t_2 + t_3 = T_s$



• $t_1, t_2, t_3 \ge 0$





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Space vector modulation

- The *closest* triangle with v_1, v_2, v_3
- Define $\overline{t} = \frac{t}{T_s}$, for every modulation cycle T_s : $\overline{t}_1 v_{1,\alpha} + \overline{t}_2 v_{2,\alpha} + \overline{t}_3 v_{3,\alpha} = v_{\alpha}^*$ $\overline{t}_1 v_{1,\beta} + \overline{t}_2 v_{2,\beta} + \overline{t}_3 v_{3,\beta} = v_{\beta}^*$ $\overline{t}_1 + \overline{t}_2 + \overline{t}_3 = 1$



• $\overline{t}_1, \overline{t}_2, \overline{t}_3 \ge 0$





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Proposed modulation method

- Online adaptive SVM
- Geometrically, *any* triangle (convex combination) containing v^* possible instead of the *closest* one
- The *voltage* and *current paths*

$$V^* = \begin{bmatrix} v_1^* \\ \vdots \\ v_L^* \end{bmatrix} \text{ and } I = \begin{bmatrix} i_1 \\ \vdots \\ i_L^* \end{bmatrix}$$

• The 'best' triangle chosen that improves loss-THD trade-off







Proposed modulation method (cont'd)

- *Optimization* window *L*
- For each p-th modulation cycle T_s ,

$$f_{p} = w_{loss,p} \left(\sum_{q=1}^{3} \sum_{r=a,b,c} E_{p,q,r} \right)^{2} + w_{THD,p} \left(\sum_{q=1}^{3} e_{p,q,\alpha}^{2} + e_{p,q,\beta}^{2} \right)$$

• Choose switching sequence which minimizes $f = \sum_{p=1}^{L} f_p$

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Neutral-point voltage balancing

• How does neutral-point *voltage* behave?

$$\frac{dv_n}{dt} = -\frac{1}{2X_C}i_n$$



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- Neutral-point *current* drawn only if phase connected to neutral-point $i_n = (1 |u_a|)i_a + (1 |u_b|)i_b + (1 |u_c|)i_c$
- Predict using *forward Euler* $v_n(t + \Delta t) = v_n(t) + \Delta t \cdot -\frac{1}{2X_c}i_n$

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Proposed modulation method (cont'd)

- *Optimization* window *L*
- For each p-th modulation cycle T_s ,

$$f_{p} = w_{loss,p} \left(\sum_{q=1}^{3} \sum_{r=a,b,c} E_{p,q,r} \right)^{2} + w_{THD,p} \left(\sum_{q=1}^{3} e_{p,q,\alpha}^{2} + e_{p,q,\beta}^{2} \right) + w_{\nu_{n},p} \nu_{n,p}^{2}$$

- Choose switching sequence which *minimizes* $f = \sum_{p=1}^{L} f_p$
- Weights depend whether $v_{n,p}$ within **bounds**
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Proposed modulation method (cont'd)

- Integer optimization problem
- 3L decision variables, each with 27 vectors, so 27^{3L} possible combinations
- Solved using *branch and bound* method
- Every *node* represents a triangle (3 vectors)



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Field-oriented control



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Loss-THD trade-off

- *SVM* (dash-dotted squares) vs *oaSVM* (solid circles)
- For L = 1, speed $\omega_r = 0.1$ pu (left) and $\omega_r = 0.4$ pu (right),

Parameter	Value
w _{loss}	1
W _{THD}	320
W _{vn}	$1 \cdot 10^{9}$
$v_{n,min}$	-0.04 pu
v _{n,max}	0.04 pu







Loss-THD trade-off (cont'd)

- *SVM* (dash-dotted squares) vs *oaSVM* (solid circles)
- For L = 1, speed $\omega_r = 0.7$ pu (left) and $\omega_r = 1$ pu (right)
- Same *parameters* as before
- *Infeasibility* solvable using longer optimization windows



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Space vector modulation

- For speed $\omega_r = 0.4$ pu, load $T_l = 1$ pu
- Same *parameters* as before



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Online adaptive SVM

- For speed $\omega_r = 0.4$ pu, load $T_l = 1$ pu
- Same *parameters* as before
- Clamps at high currents, similar to discrete PWM







Online adaptive SVM (cont'd)

- For speed $\omega_r = 0.4$ pu, load $T_l = 1$ pu
- Same *parameters* as before



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Conclusion

Summary

- New modulation method *online adaptive SVM*
- Blend of *SVM* and discrete PWM, very flexible
- Improves trade-off between losses and THD
- Balances *neutral-point voltage* within bounds
- Infeasibility solvable for longer optimization windows
- High computational complexity, *brand and bound* method

Future work:

- Investigate longer *optimization window* L > 1
- Explore other *cost functions*



Thank you for your attention!

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