

Experimental Modal Analysis (EMA) on a vibration cube fixture

M. Sc. Emanuel Malek
Eindhoven – November 2017

Introduction

- Basics
- Why EMA?

Preparation and execution

- Testing variants
- Definition of measuring points/ Geometry creation
- Excitation and response

Test results

- Variant 1 (elastic suspension)
- Variant 2 (shaker armature - impulse)
- FRF Variant 1 vs. 2
- Variant 3 (shaker armature - sweep)

Summary & conclusion

SDOF System

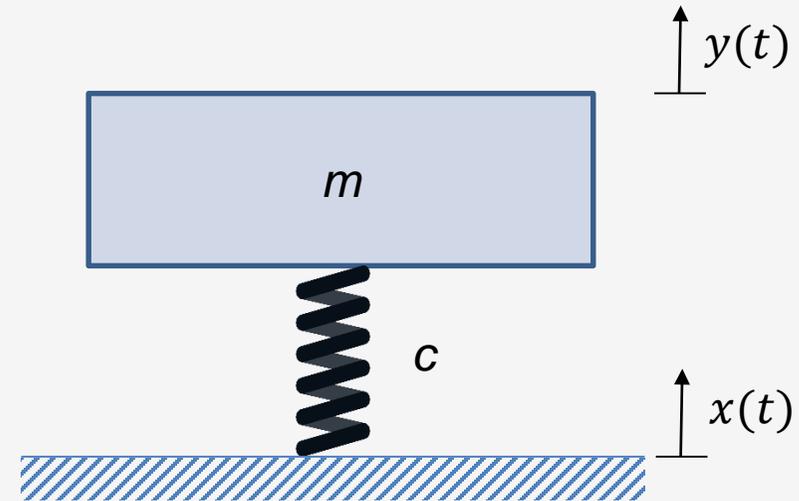
- Idealized systems, e.g.
 - Armature (shaker)
 - Piezo - Accelerometer
- One mass m [kg], one spring c [N/m]
- Owns one natural frequency (eigenfrequency)

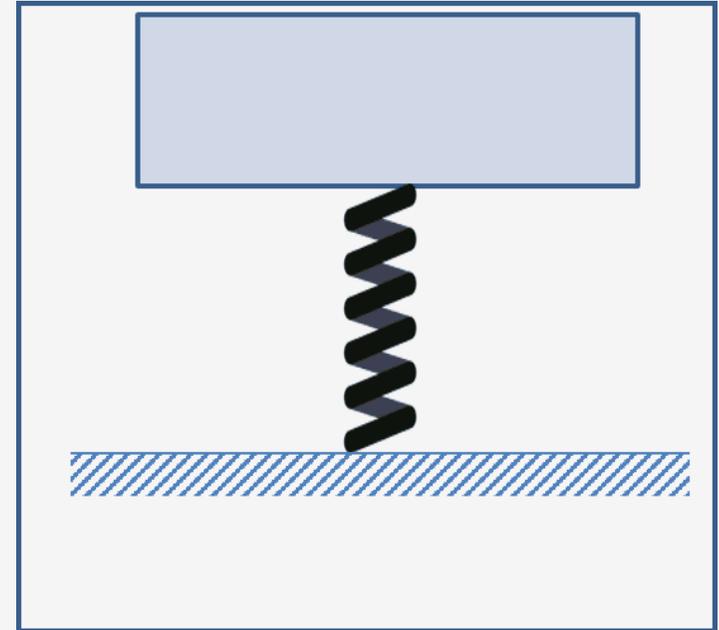
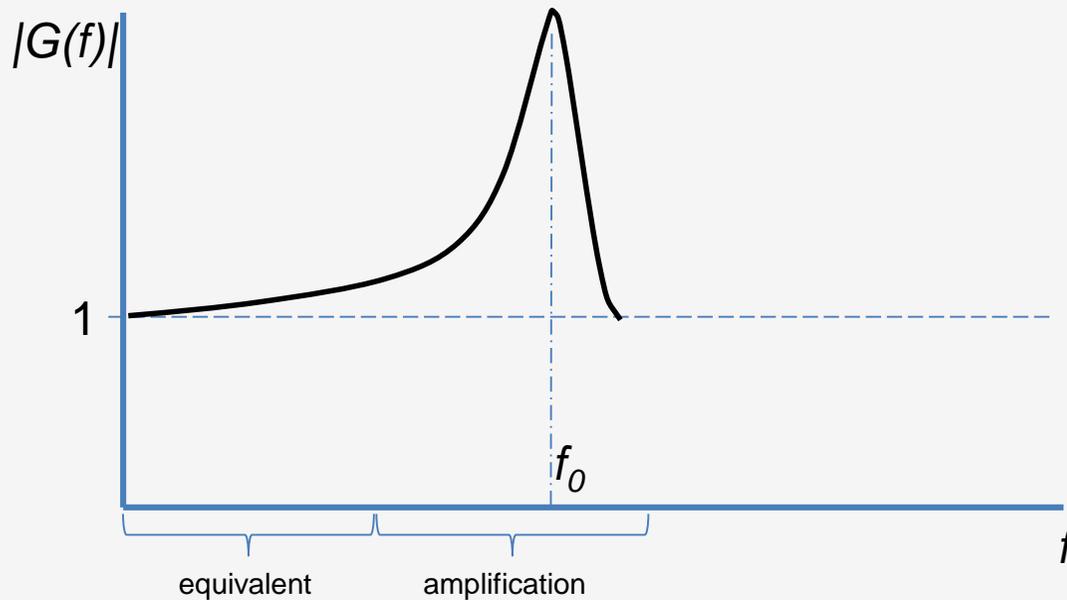
$$\circ \omega_0 = \sqrt{\frac{c}{m}} \rightarrow f_0 = \frac{\omega_0}{2\pi} = \frac{\sqrt{\frac{c}{m}}}{2\pi}$$

- „System prefers to moves at natural frequencies“

- Transmissibility function (amplification function) $G(f) = \frac{\text{Response}}{\text{Excitation}} = \frac{\hat{y}(f)}{\hat{x}(f)}$

- behavior of the movement regarding to the excitation in frequency domain
 - amplification, isolation (attenuation)



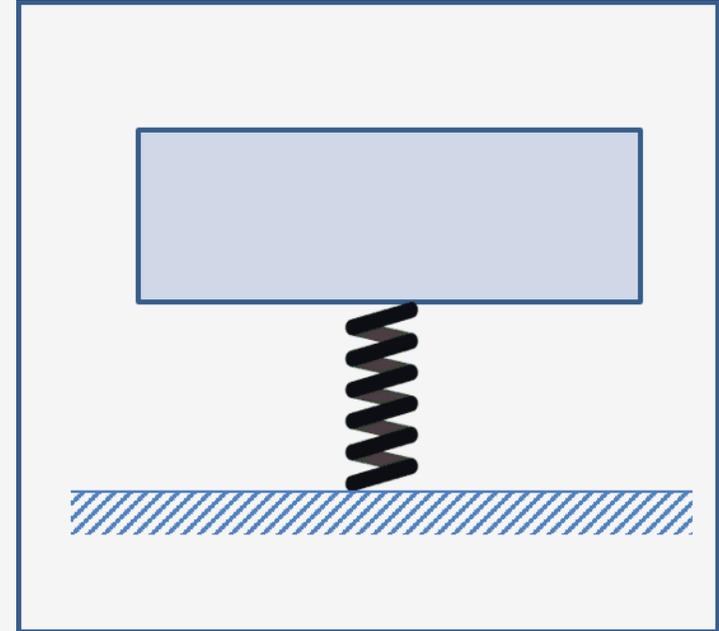
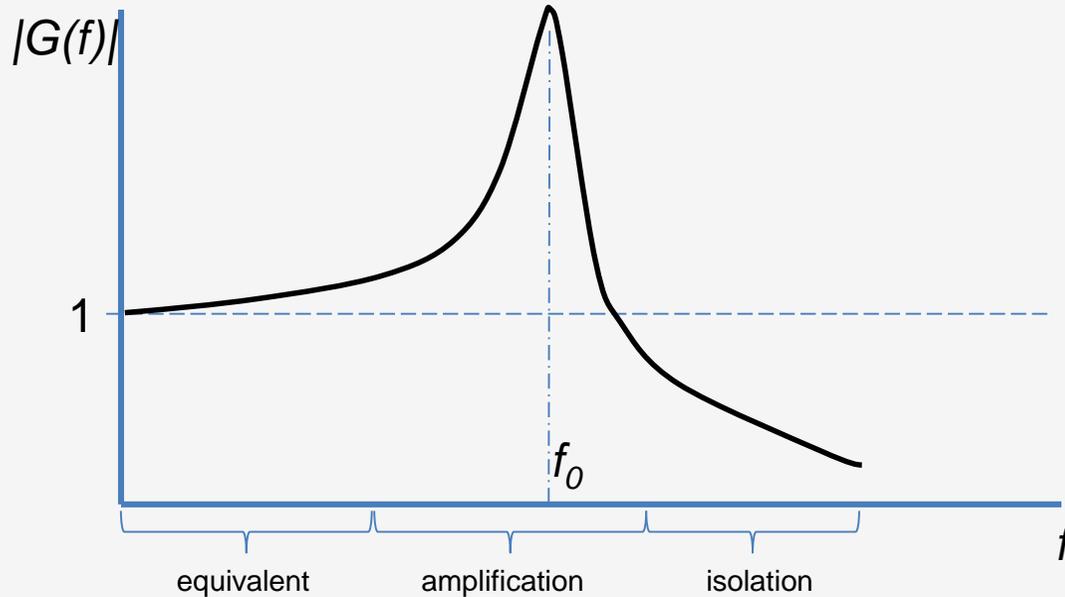


3 areas of transmissibility function

- Equivalent area $G(f) \approx 1$
- Amplification $G(f) \gg 1$
- Isolation $G(f) < 1$

Resonance

- if $f = f_0$



3 areas of transmissibility function

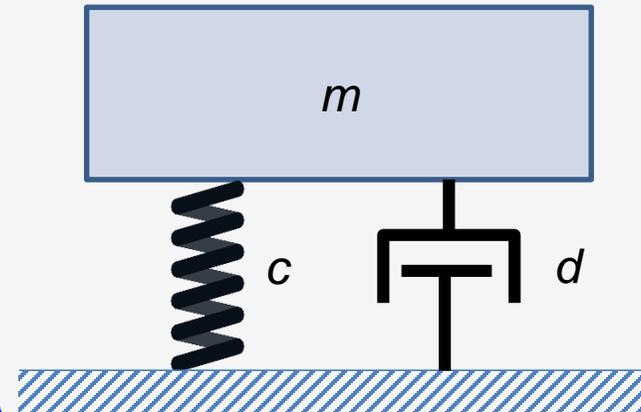
- Equivalent area $G(f) \approx 1$
- Amplification $G(f) \gg 1$
- Isolation $G(f) < 1$

Isolation

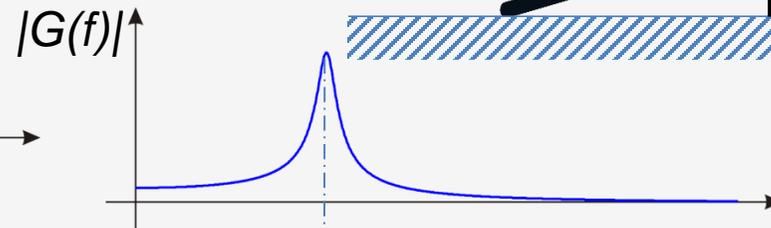
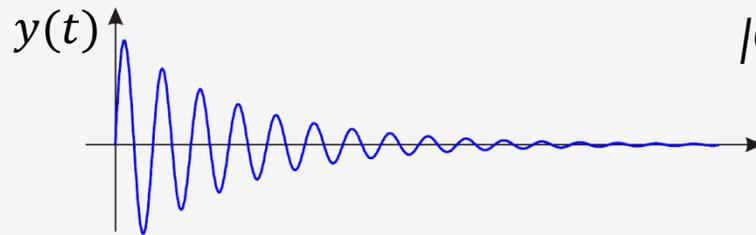
- if $f > f_0$

Damping dissipates energy

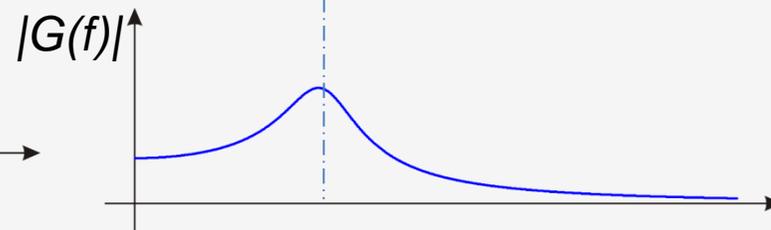
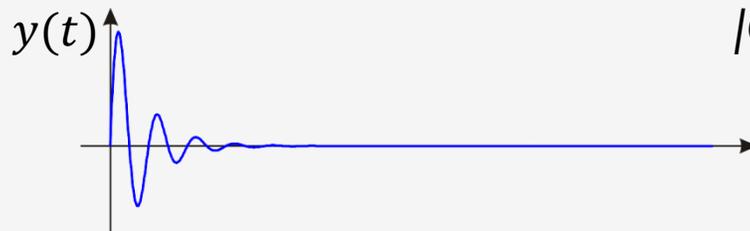
- Briefer decay time
- Damping coefficient d [$\frac{\text{kg}}{\text{s}}$ resp. $\text{N} \frac{\text{s}}{\text{m}}$]

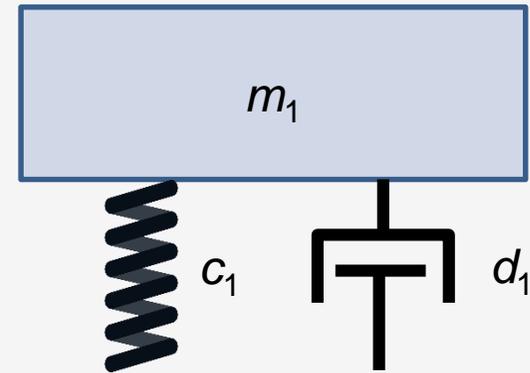
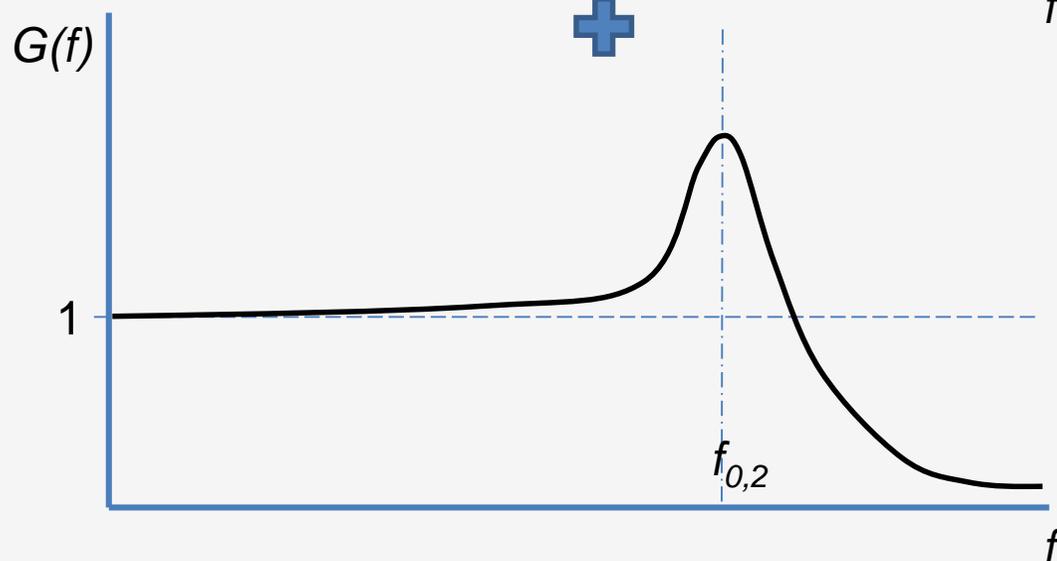
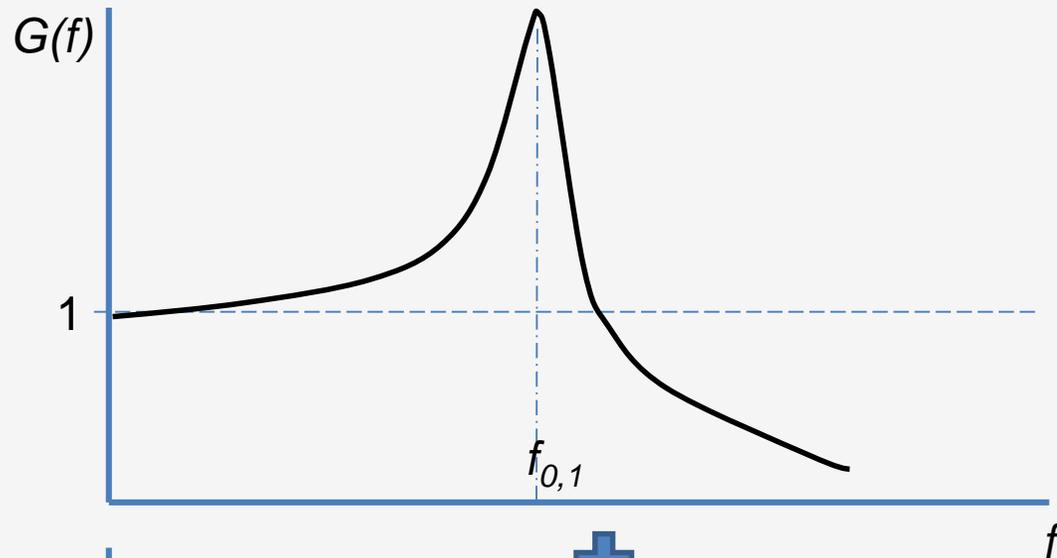


Softly damped system

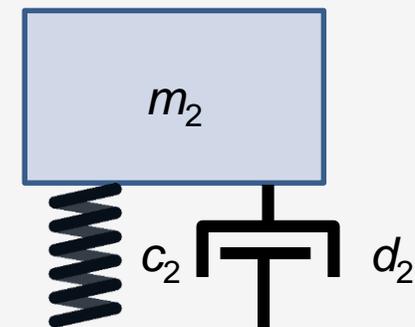


Greatly damped system



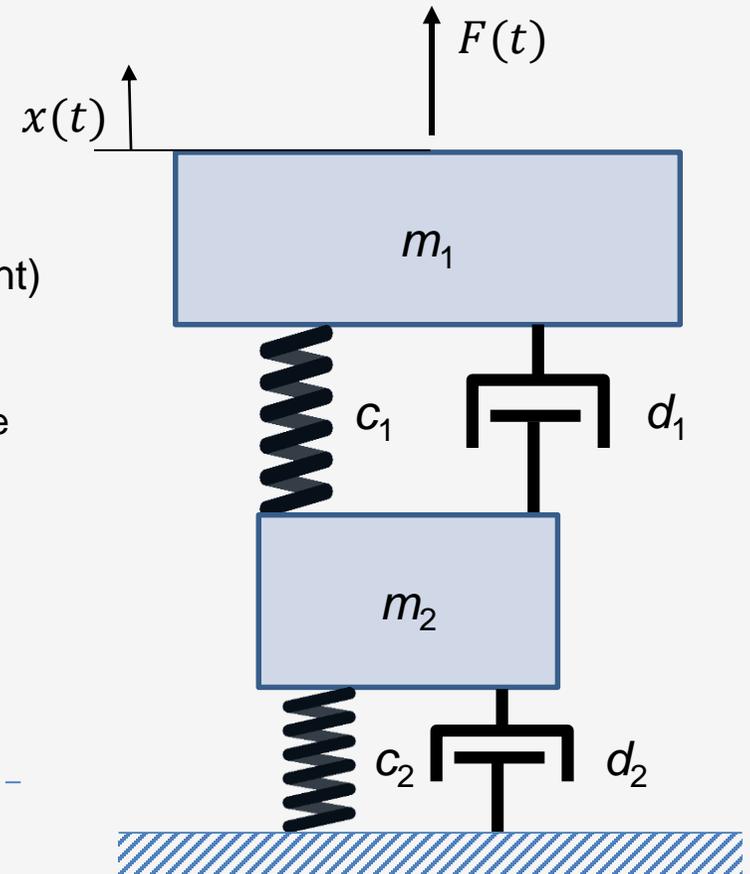
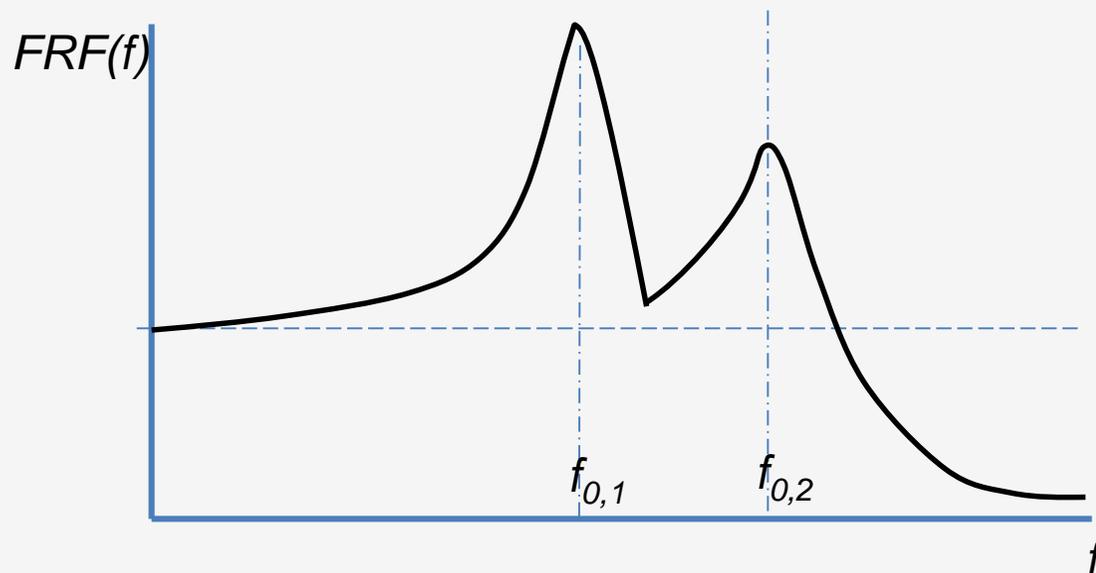


+



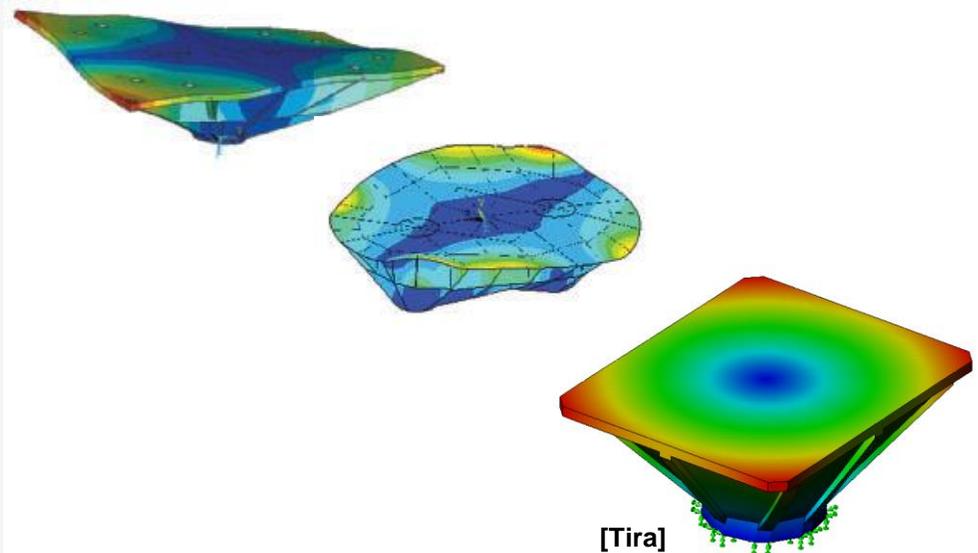
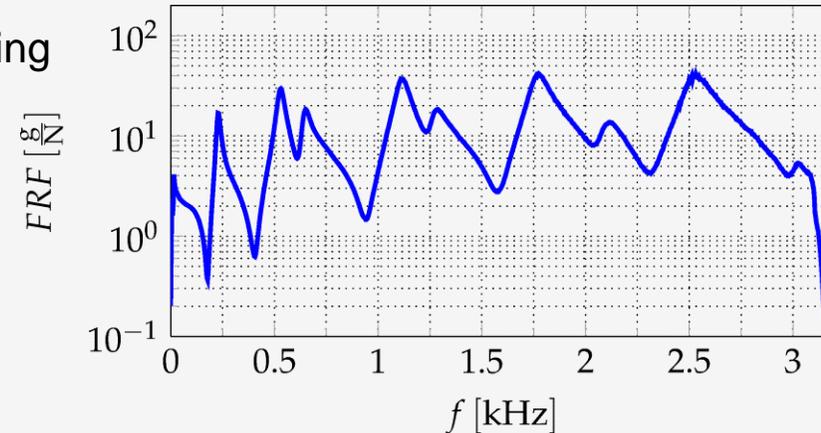
Force excited two-mass spring damper system

- Two natural frequencies
- Two natural modes
- Resonance followed by anti resonance (Drivepoint)
- FRF (Frequency Response Function)
 - Ratio of acceleration, velocity & displacement to force



Why modal analysis of fixtures and test sockets?

- Determine natural frequencies/ damping
 - Determine critical frequency range
 - Customizing test definitions
 - Notching / forcelimination
 - Design features
- Determine natural modes
 - Identification of suitable positions for control sensors, DUT
 - Design features
- FEM validation



Preparation and execution

- Testing variants

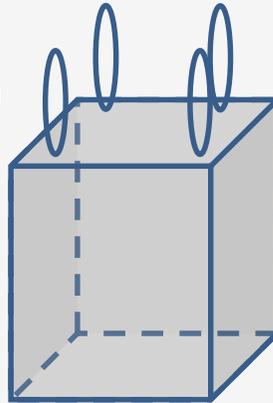
Test object: Cube fixture

Variant 1:

Elastic suspension

Excitation:

Impulse

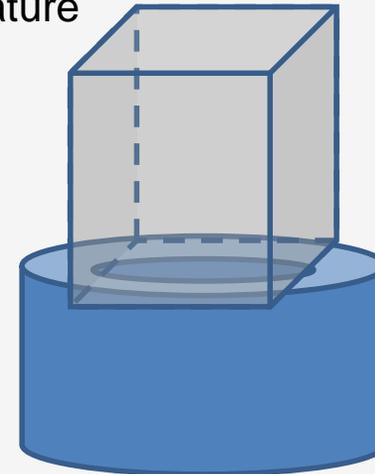


Variant 2:

Shaker armature

Excitation:

Impulse



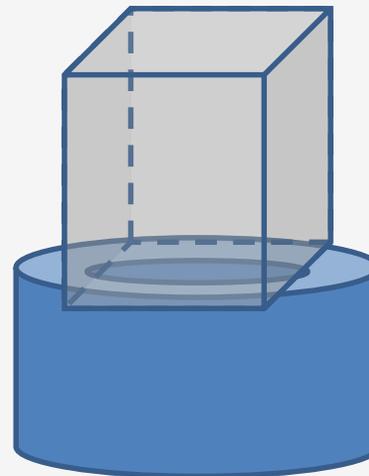
Variant 3:

Shaker armature

Excitation :

Sine sweep

(10 – 2500 Hz)

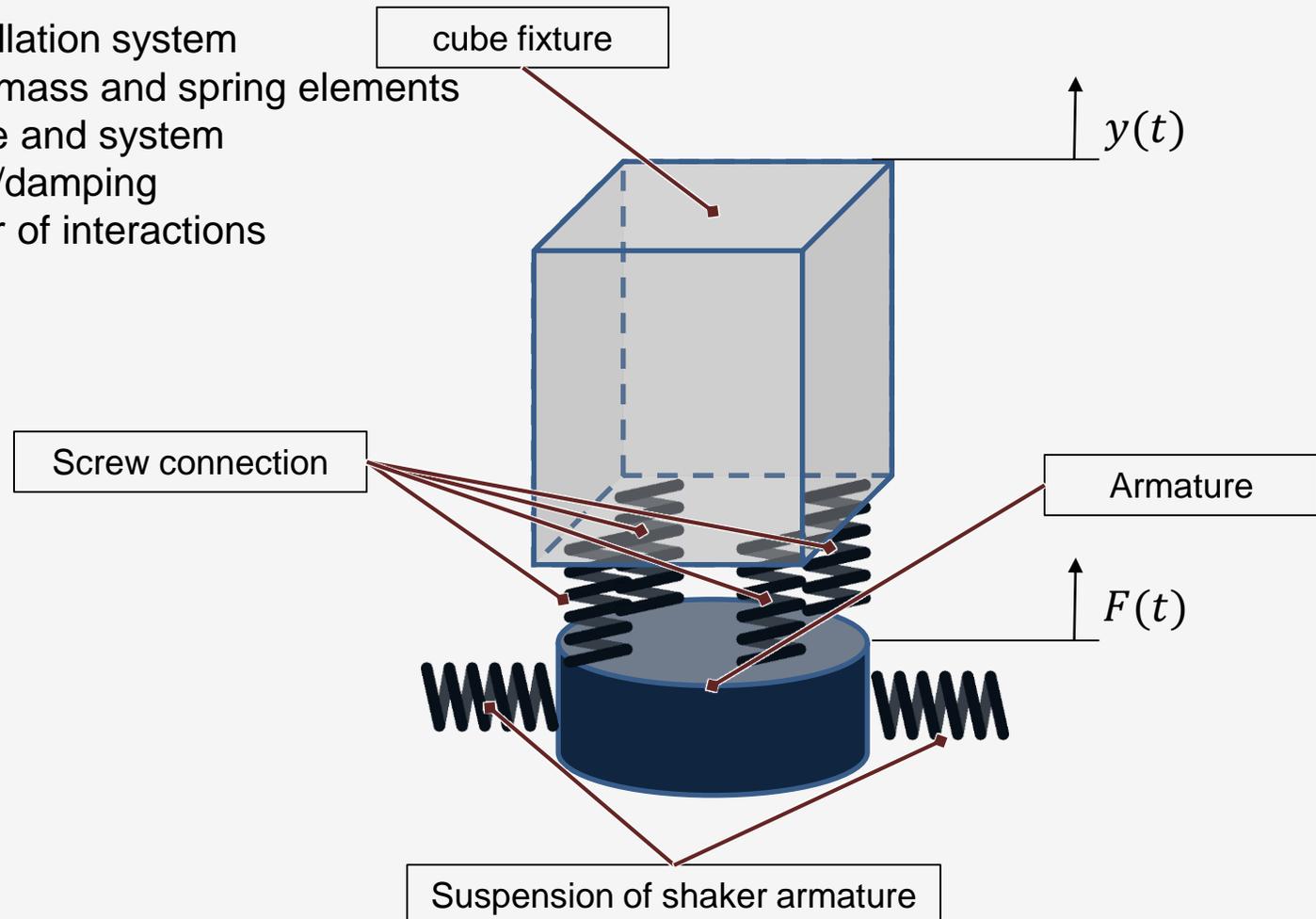


Preparation and execution

- Testing variants

Approximation system for cube fixture on shaker armature

- Complex oscillation system
 - Several mass and spring elements
 - Structure and system stiffness/damping
- Large number of interactions



Preparation and execution

- Definition of measuring points/ Geometry creation

Test object:

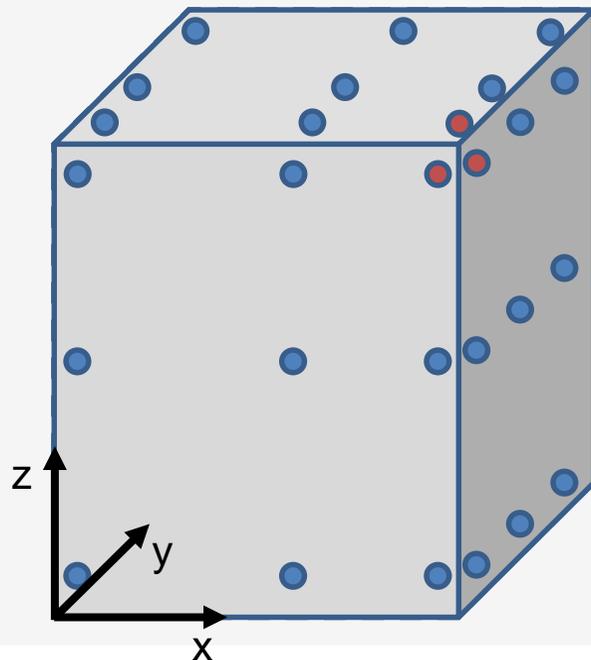
Cube fixture

- Symmetrical
- Mass approx. 58 kg

Measuring points:

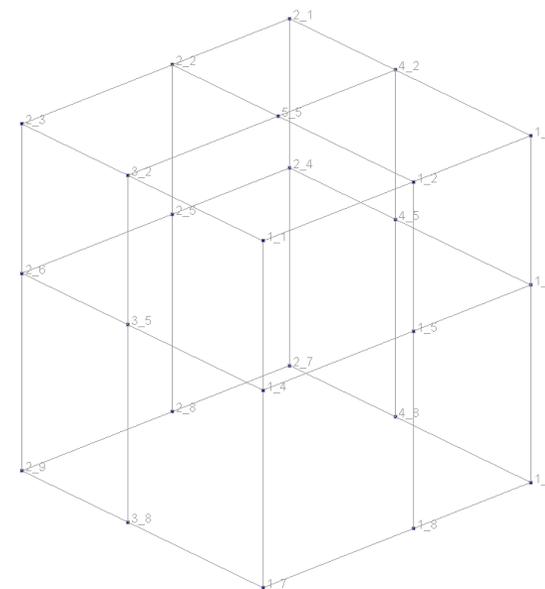
- 9 Accelerometer per face
→ 45 Measuring points
- Merging of corner points
(m+p Analyzer)
→ 3-Dimensionale dynamic

Vorüberlegung bzw. Positionsmessung



Excel Table,
STL-Format

m+p Analyzer Messpunkt-Geometrie

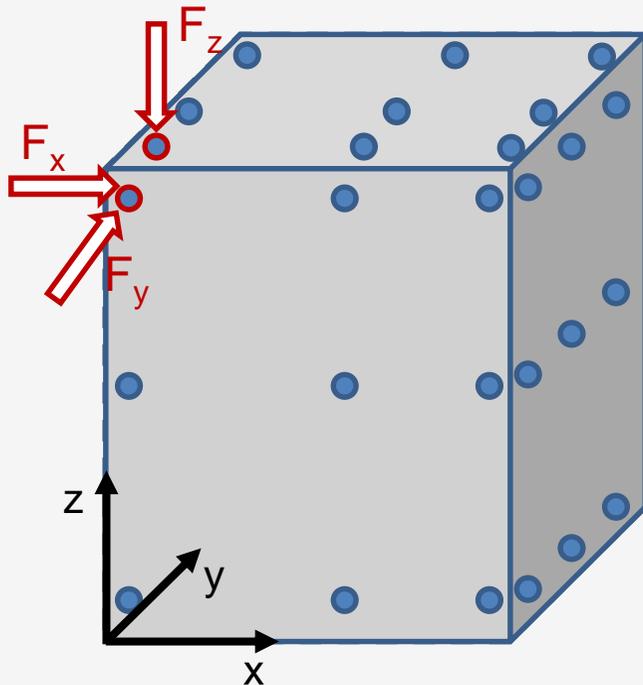


Preparation and execution

- Excitation & response

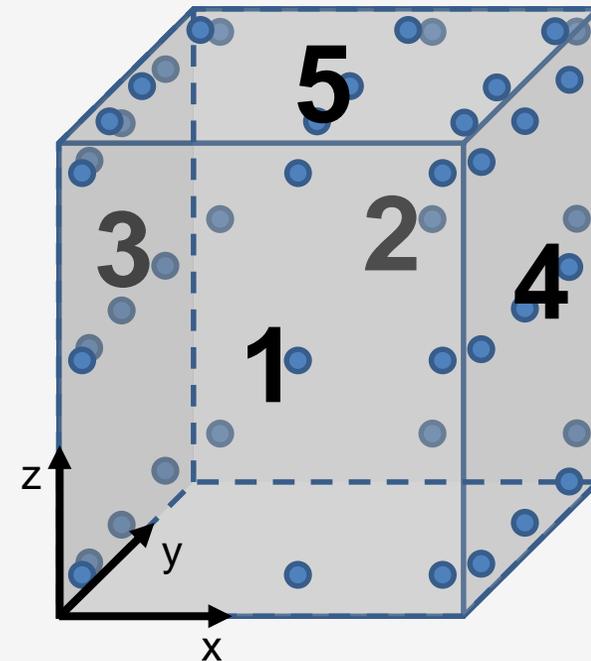
Impulse excitation:

- 3 Drivepoints
- F_x in $+x$, F_y in $+y$, F_z in $-z$
- Impulse hammer with hard plastic tip (0,23 mV/N)
- roving



Impulse response:

- Accelerometer (100 mV/g)
- Measuring direction of points on Surface:
 - 1: $-y$, 2: $+y$, 3: $-x$, 4: $+x$, 5: $+z$
- fixed

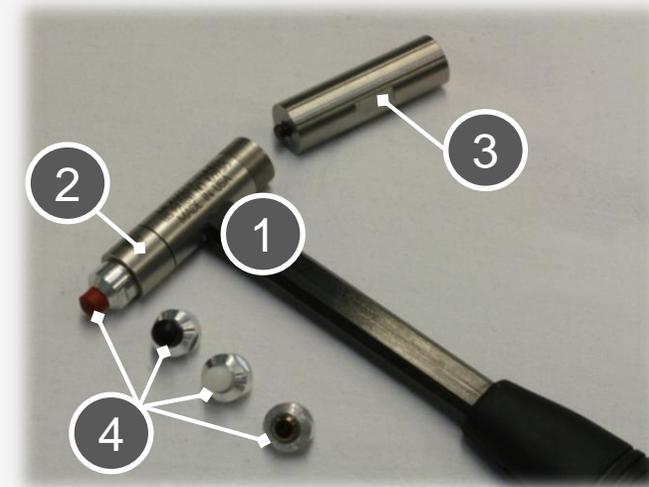


Preparation and execution

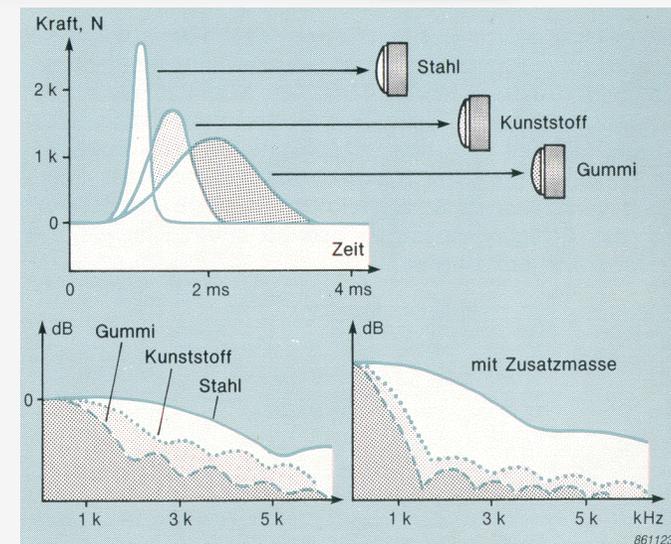
- Excitation & response

Impulse excitation:

- Hammer (1)
- Force transducer (2)
- Additional mass (3)
- Hammer tip (4)
- Mass of hammer reaches from a few grams up to several Kilograms
- Excitation frequencies:
 - From 100 Hz
(Heavy Hammer, soft tip)
 - To more than 50 kHz
(Light Hammer, hard tip).



[PCB]



[B&K]

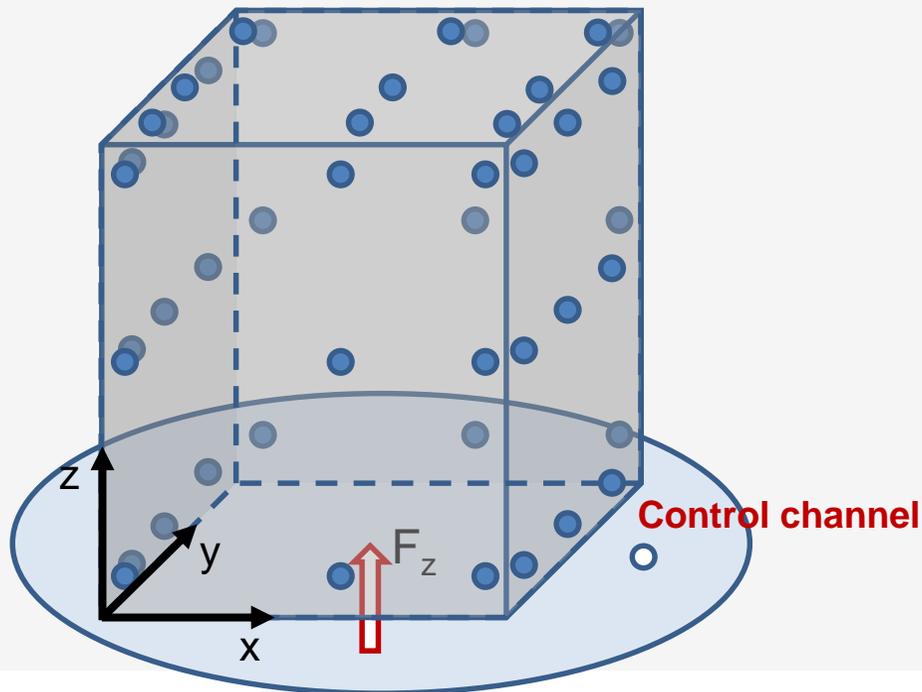
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Preparation and execution

- Excitation & response

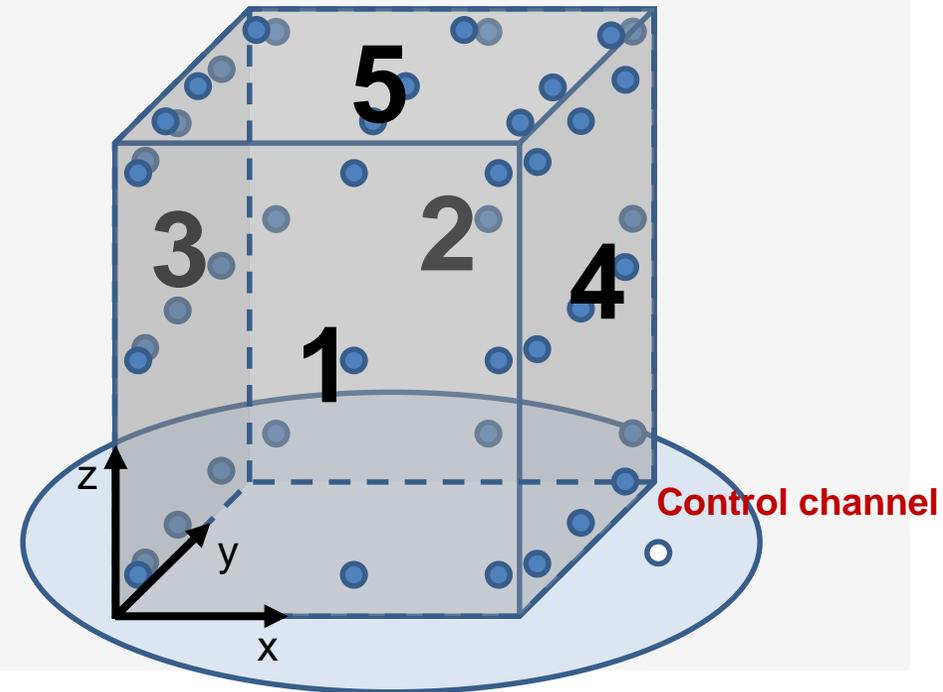
Sine-Sweep-Excitation:

- F_z in +z (Cube on shaker armature)
- Control channel delivers excitation signal
- 10-2500 Hz
- 1g constant
- 1 Octave/min



Impulse response:

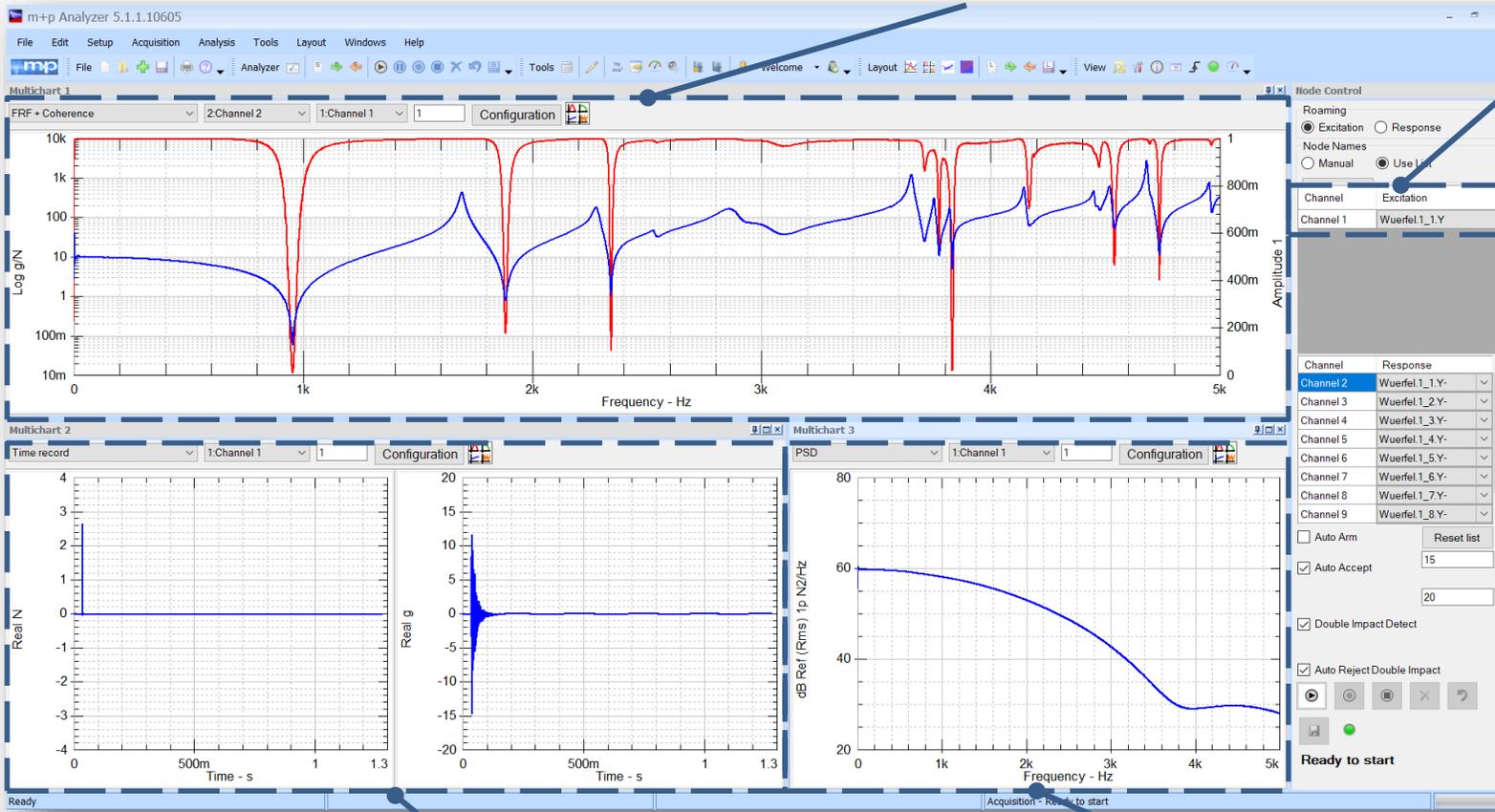
- Accelerometers (100 mV/g)
- Measuring direction of points on Surface:
 - 1: -y , 2: +y, 3: -x, 4: +x, 5:+z
- fix



Preparation and execution - Excitation & response

Monitoring during impulse hammer test

FRF (*Frequency Response Function* [g/N]) + Coherence of Drivepoint



Display:
Excitation
point

Time signal of excitation
and response

PSD (Power spectrum density)
of hammer impulse

Preparation and execution

- Excitation & response, evaluable frequency range

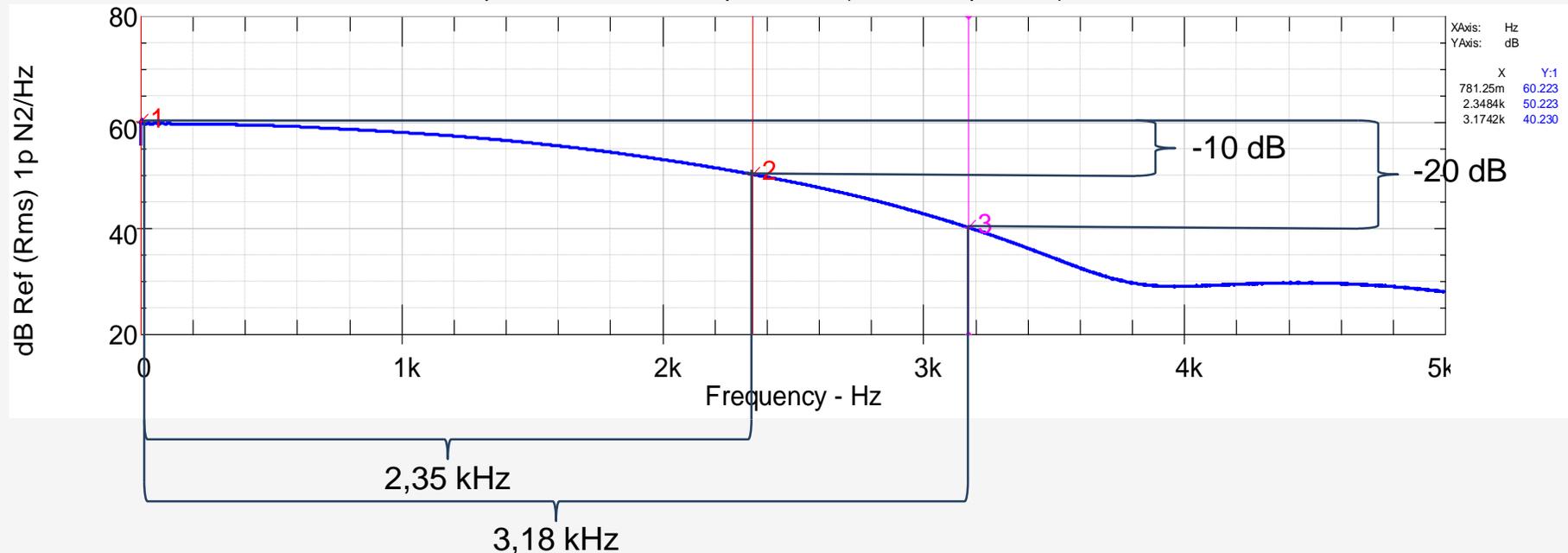
Measured signals:

- Time signals, PSD, FRF, Coherence

Evaluable frequency range for modal parameters:

- f_{\min} for elastic suspension \rightarrow 0,8 Hz (longer time window)
- f_{\min} for cube on shaker armature \rightarrow 1,6 Hz (shorter time window)
- f_{\max} depends on impulse decrease (10-20 dB difference)
 - Additional considering of coherence

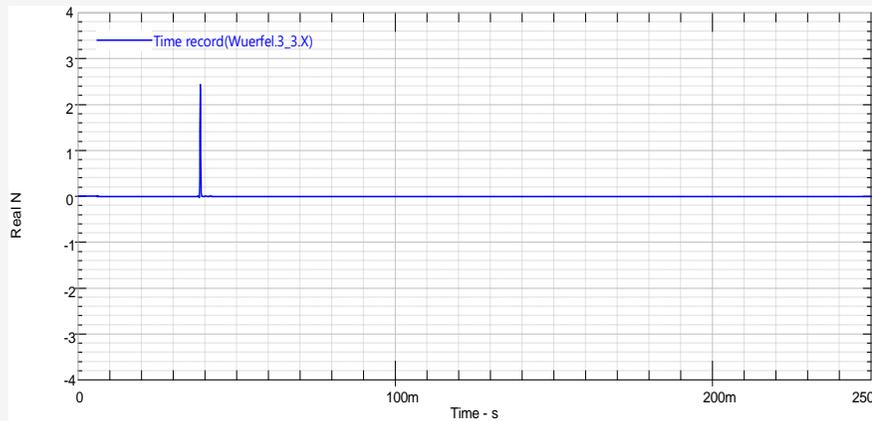
Bsp. PSD of hammer impulse in Y (elastic suspension)



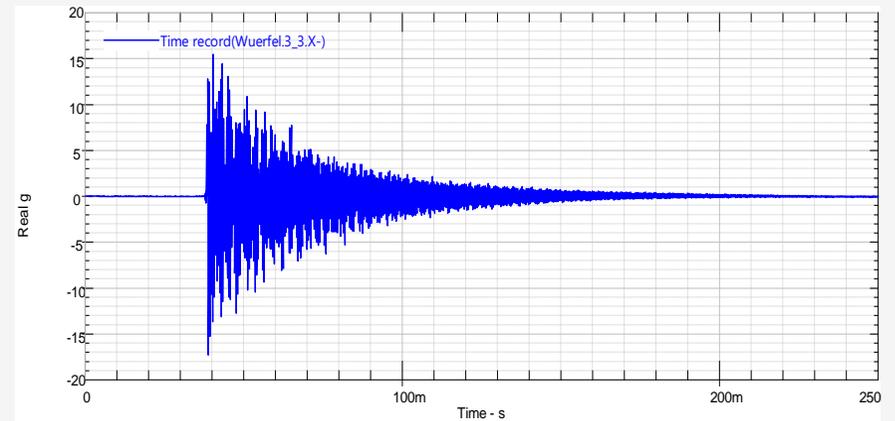
Test results

- Test variant 1 (elast. suspension), Impact in +X

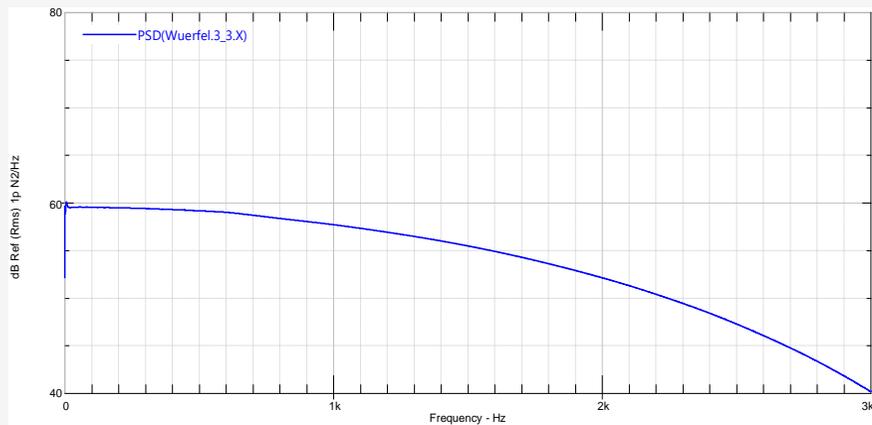
Excitation: Force impulse in time domain



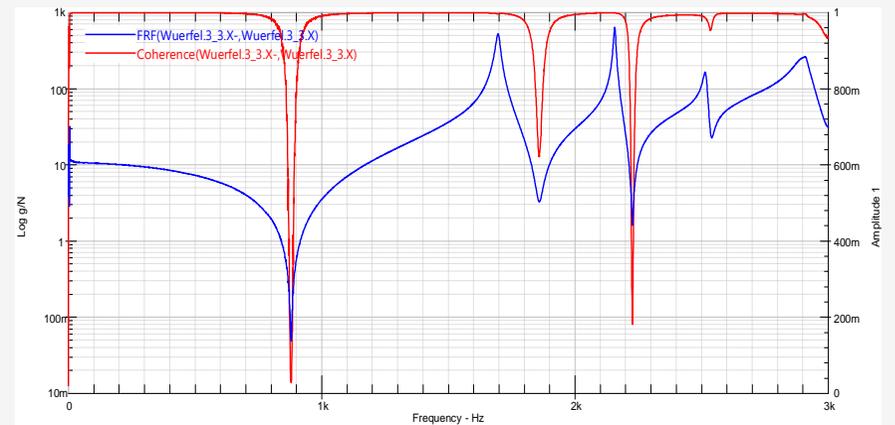
Response: Accel. in time domain



Excitation: Force impulse in frequency domain



FRF and coherence function

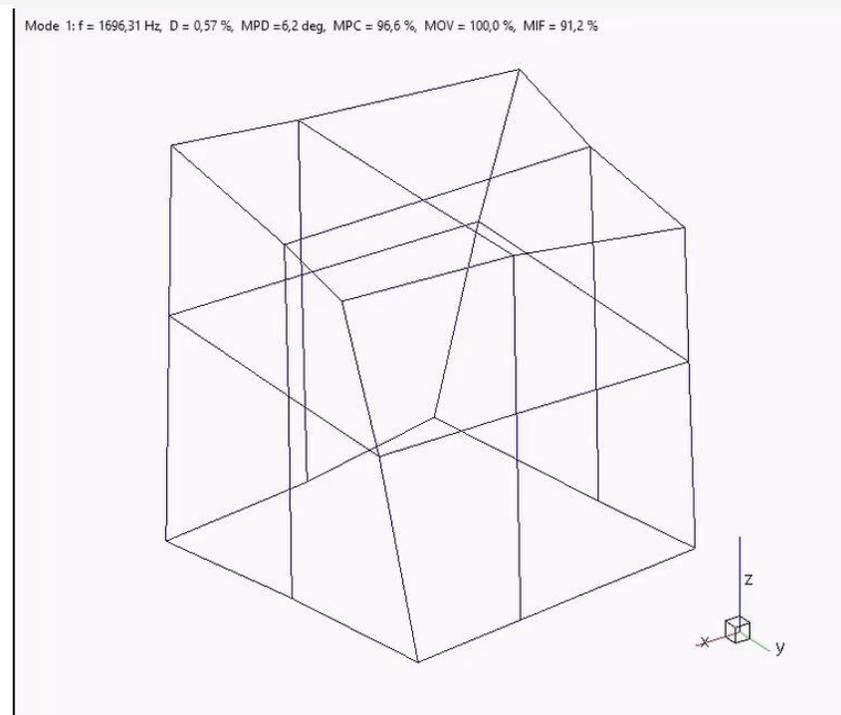
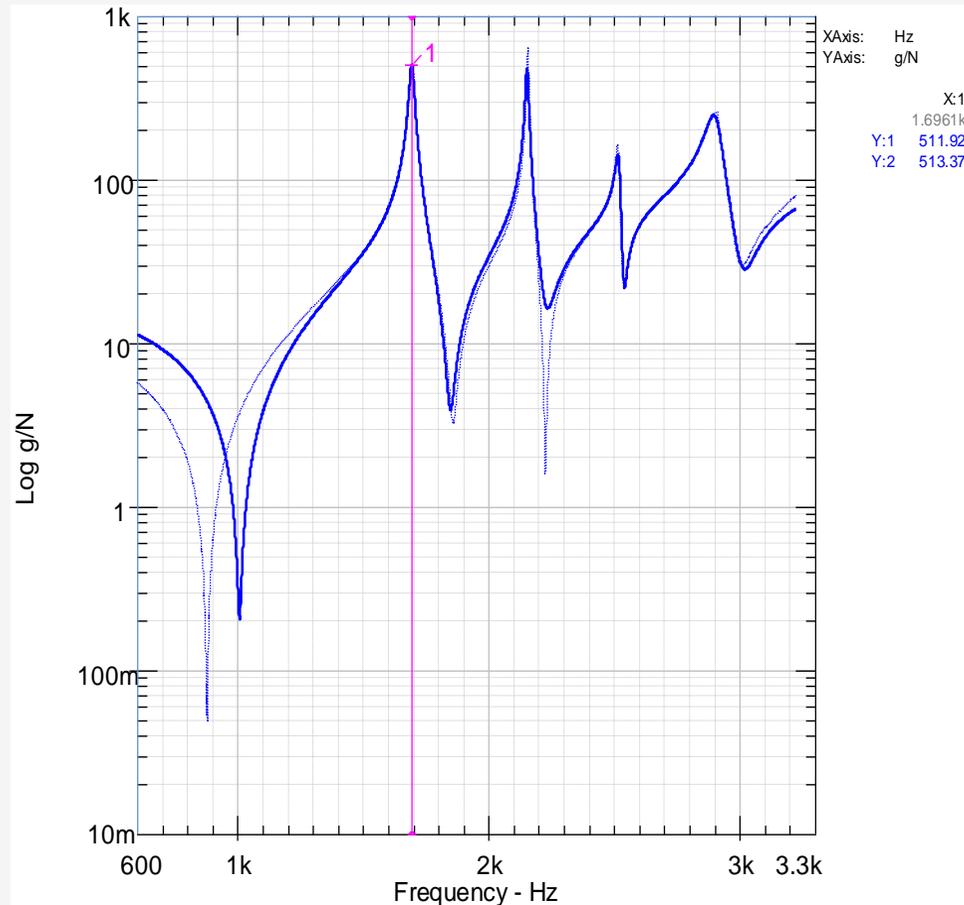


Test results

- Test variant 1 (elast. suspension), Impact in +X

1. Mode: Torsional mode (compare excitation in Y, Z)

Frequency: 1696,3 Hz, Damping: 0,57%; Mode Indicator Function (MIF): **91,2%**

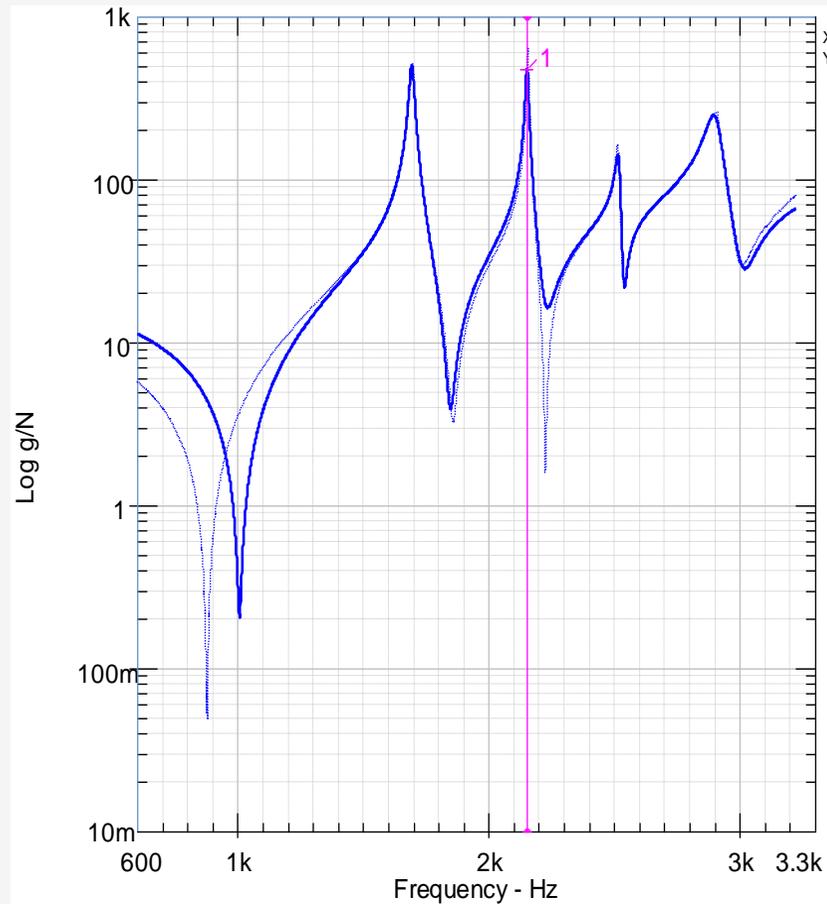


Test results

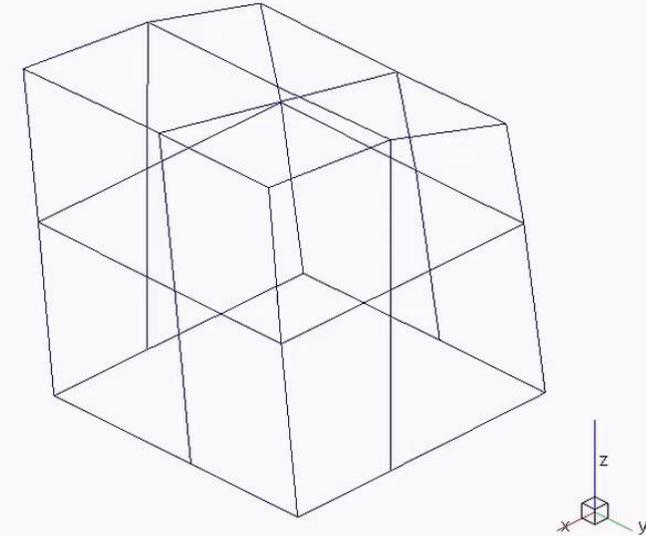
- Test variant 1 (elast. suspension), Impact in +X

2. Mode: Shear mode (compare excitation in Z)

Frequency: 2155 Hz, Damping: 0,29%; Mode Indicator Function (MIF): **70%**



Mode 2: f = 2154,96 Hz, D = 0,29 %, MPD = 16,4 deg, MPC = 76,2 %, MOV = 99,9 %, MIF = 69,7 %

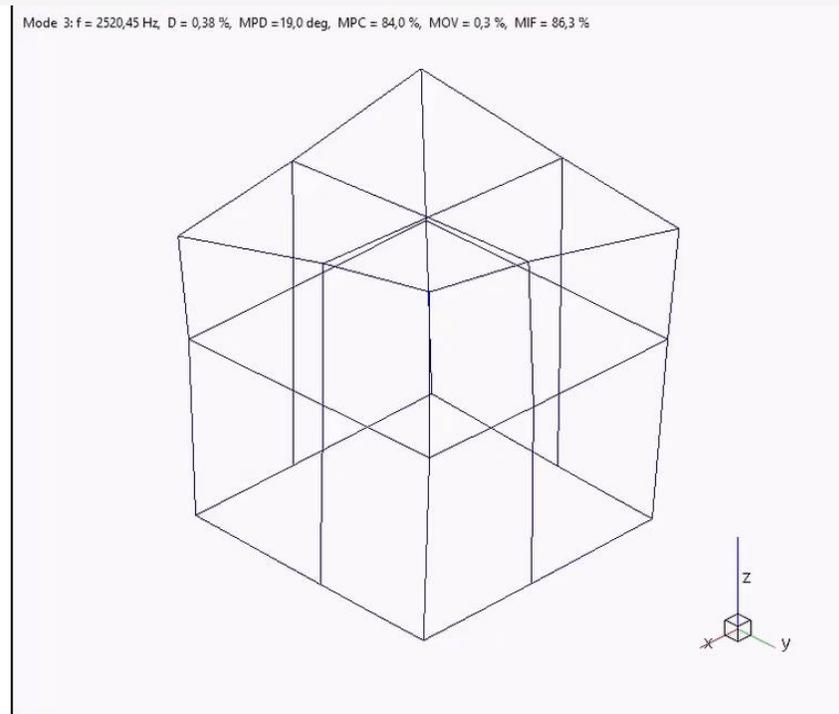
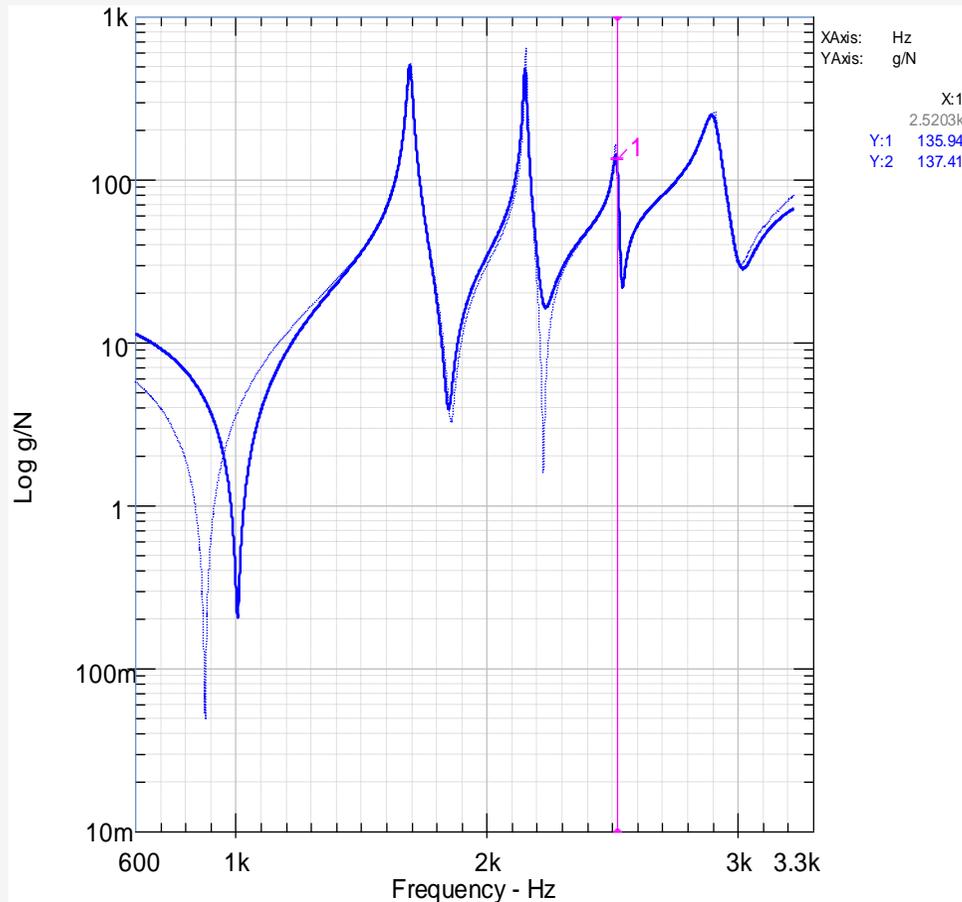


Test results

- Test variant 1 (elast. suspension), Impact in +X

4. Mode (compare excitation in Y,Z)

Frequency: 2520 Hz, Damping: 0,38%; Mode Indicator Function (MIF): **86,3%**

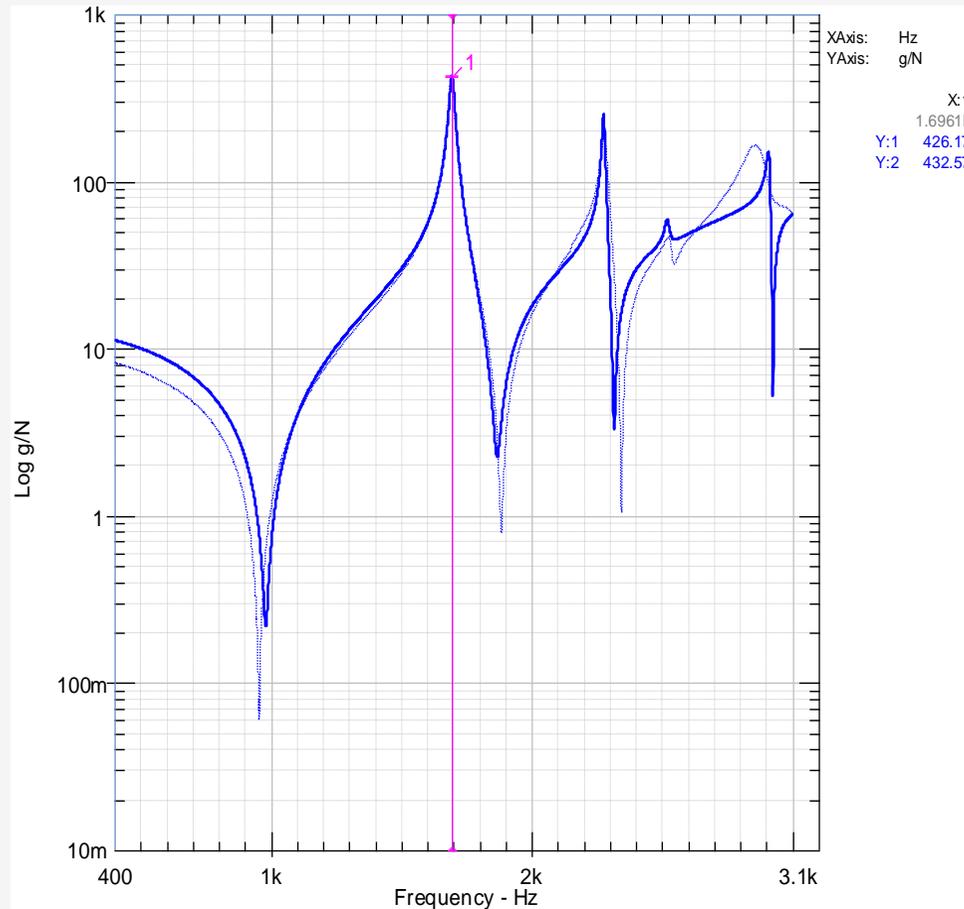


Test results

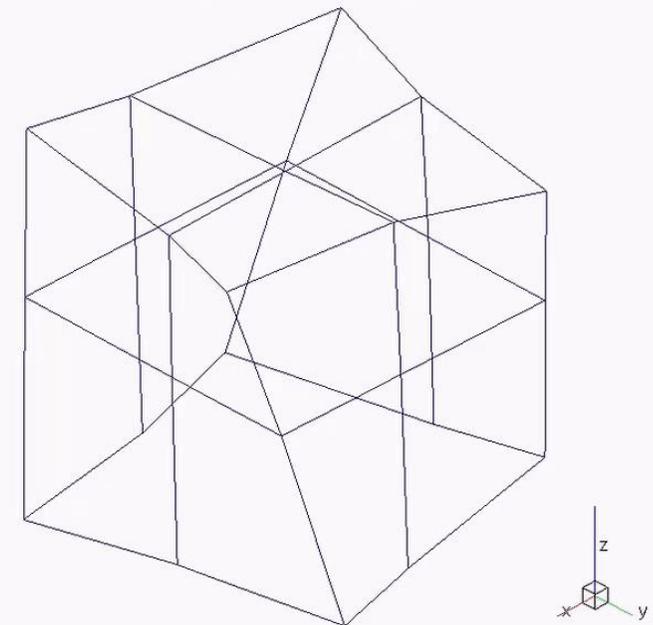
- Test variant 1 (elast. suspension), Impact in +Y

1. Mode: Torsional mode (compare excitation in X,Z)

Frequency: 1696 Hz, Damping: 0,58%; Mode Indicator Function (MIF): **93,9%**



Mode 1: f = 1696,07 Hz, D = 0,58 %, MPD = 6,2 deg, MPC = 97,4 %, MOV = 100,0 %, MIF = 93,9 %

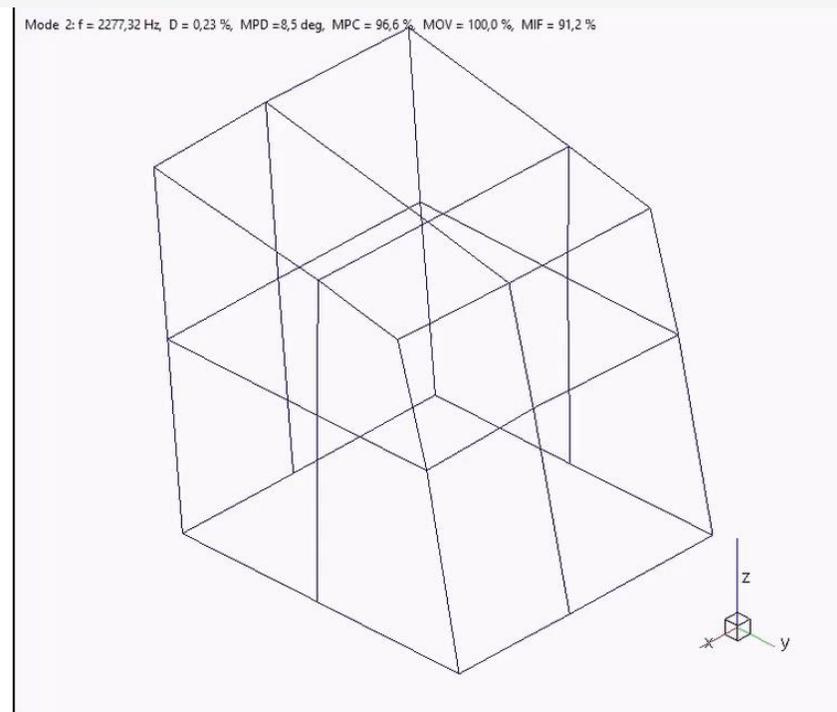
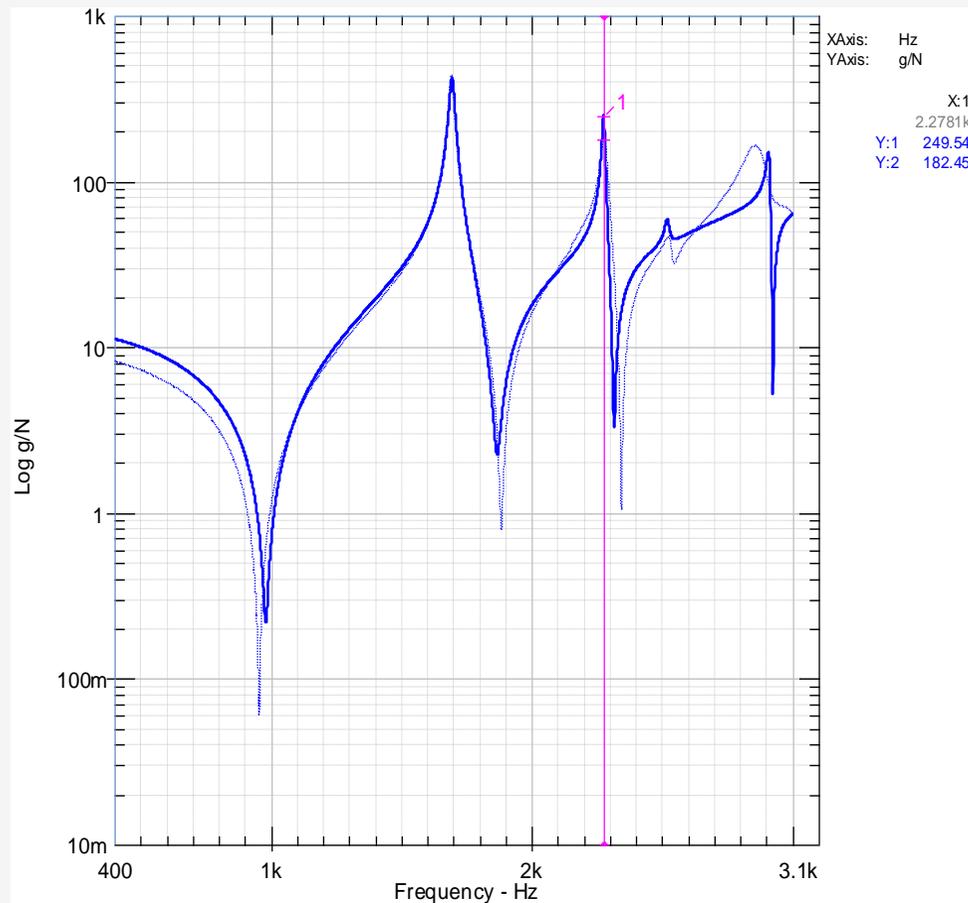


Test results

- Test variant 1 (elast. suspension), Impact in +Y

3. Mode: Shear mode (compare excitation in Z)

Frequency: 2277,3 Hz, Damping: 0,23%; Mode Indicator Function (MIF): **91,2%**

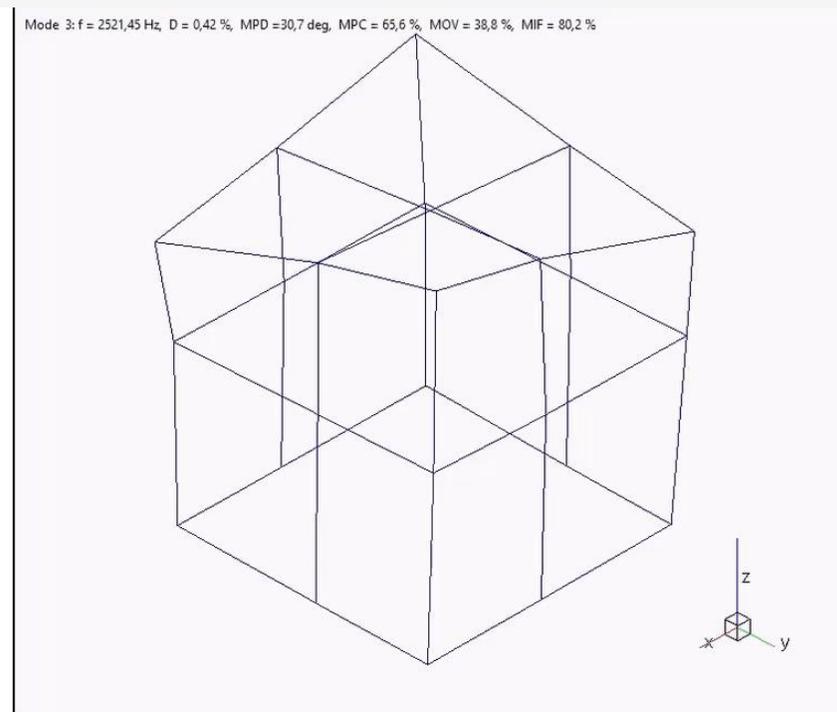
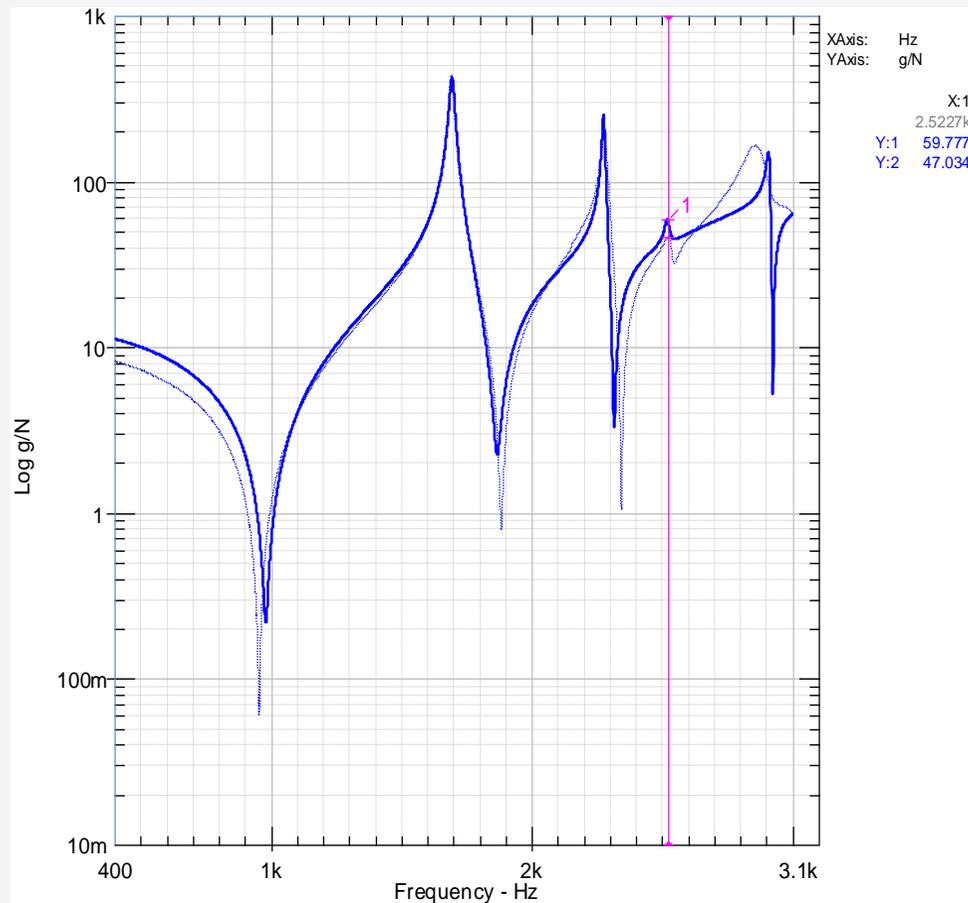


Test results

- Test variant 1 (elast. suspension), Impact in +Y

4. Mode (compare excitation in X,Z)

Frequency: 2521,5 Hz, Damping: 0,42%; Mode Indicator Function (MIF): **80,2%**

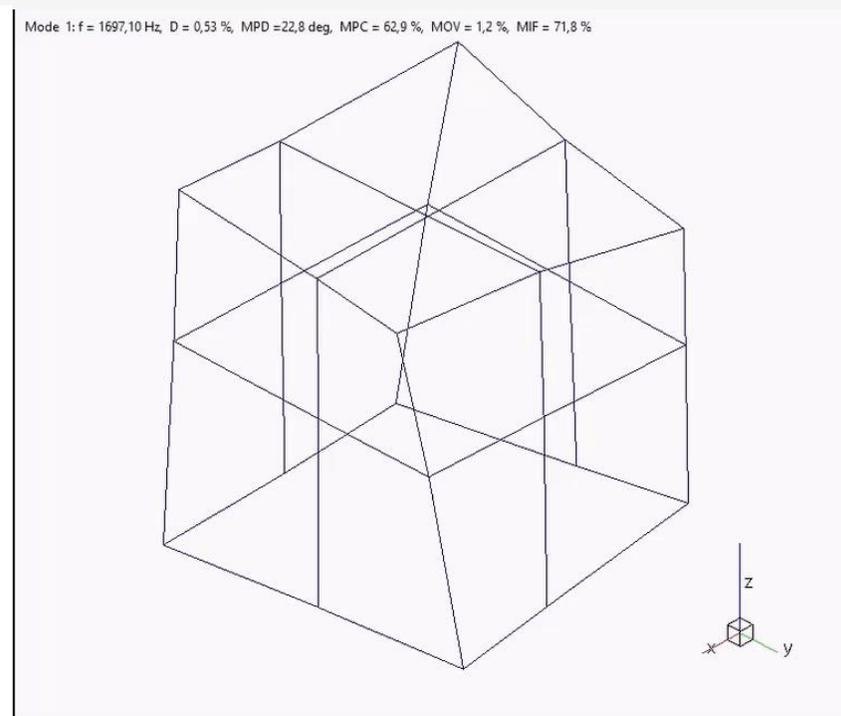
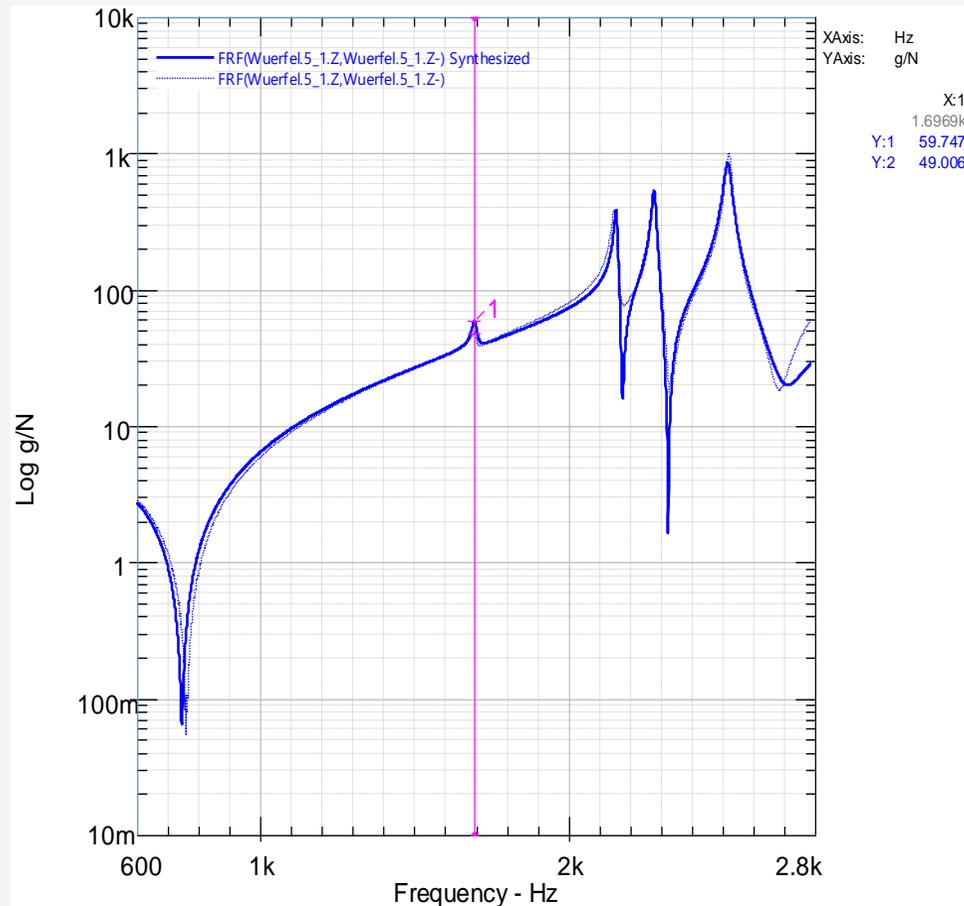


Test results

- Test variant 1 (elast. suspension), Impact in -Z

1. Mode: Torsional mode (compare excitation in X,Y)

Frequency: 1697,1 Hz, Damping: 0,53%; Mode Indicator Function (MIF): **71,8%**

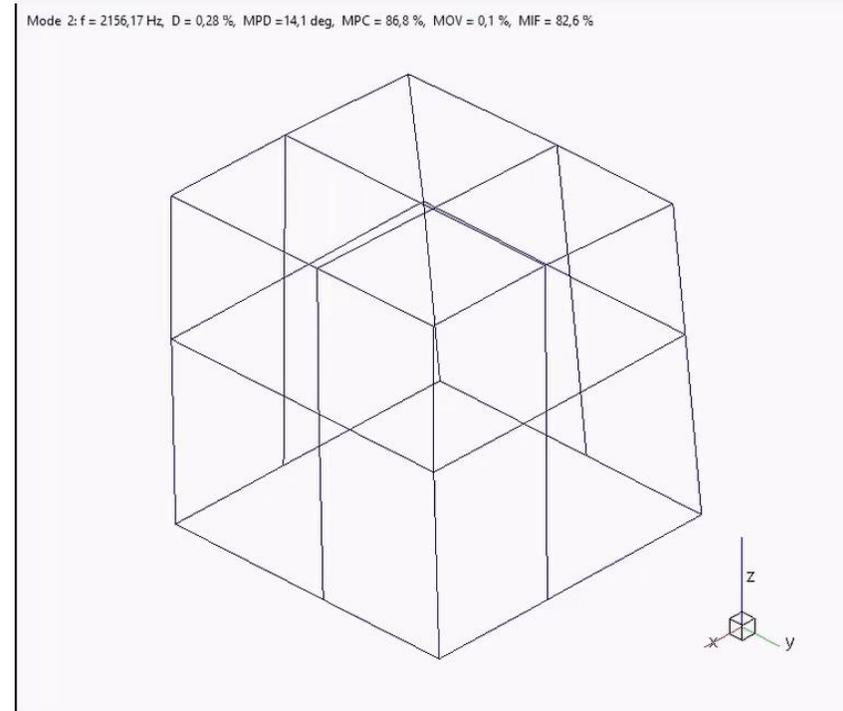
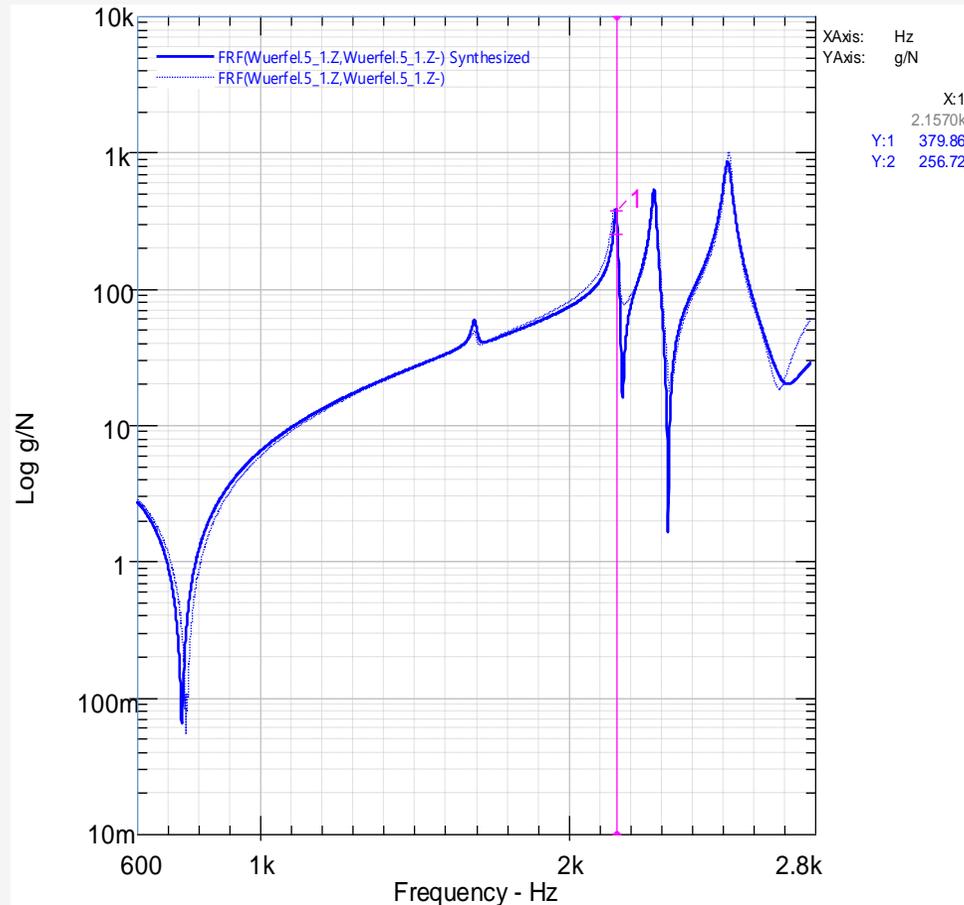


Test results

- Test variant 1 (elast. suspension), Impact in -Z

2. Mode: Shear mode (compare excitation in X,Y)

Frequency: 2156,2 Hz, Damping: 0,28%; Mode Indicator Function (MIF): **82,6%**

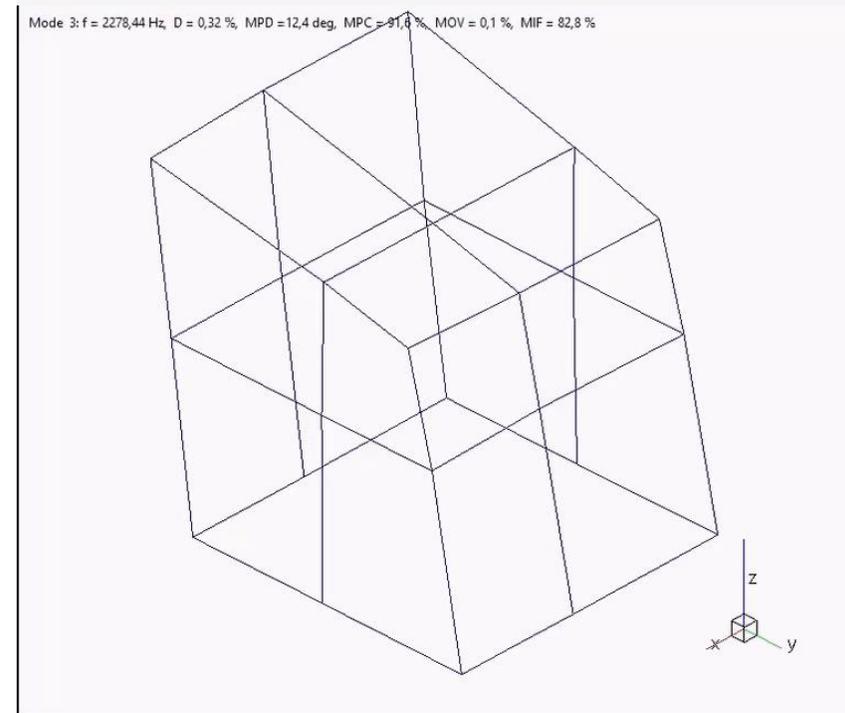
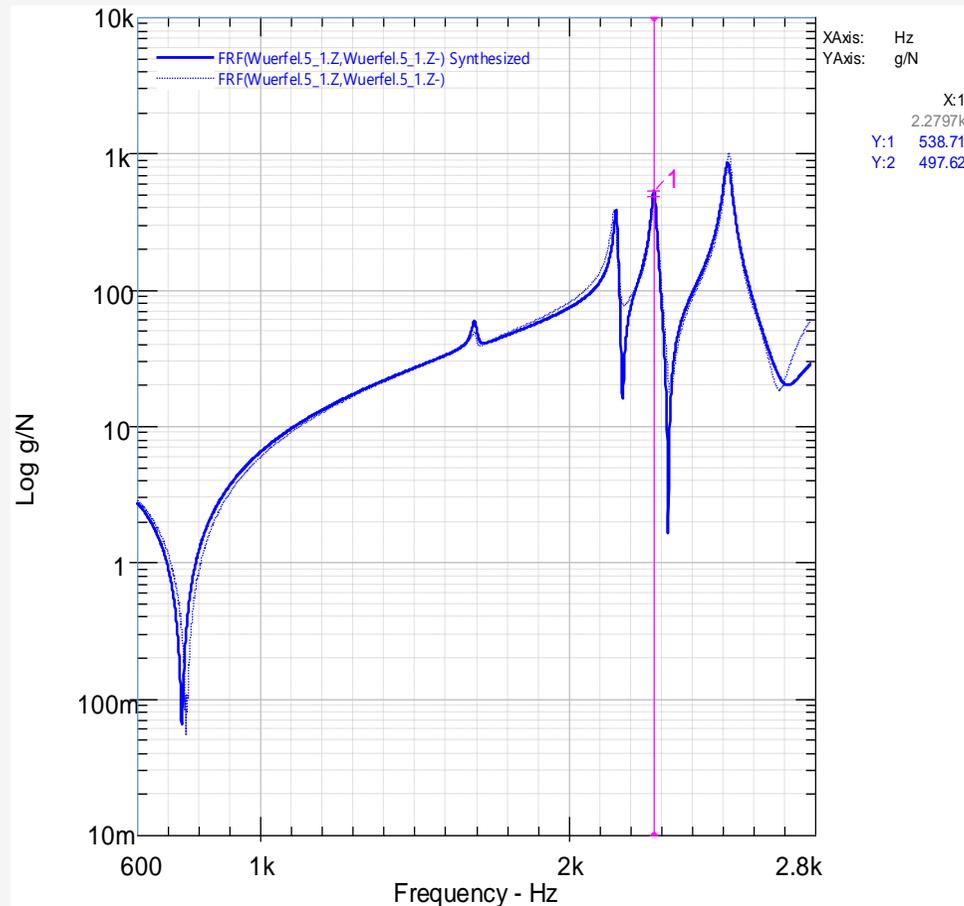


Test results

- Test variant 1 (elast. suspension), Impact in -Z

3. Mode: Shear mode (compare excitation in X,Y)

Frequency: 2278,4 Hz, Damping: 0,32%; Mode Indicator Function (MIF): **82,8%**



Test results

- Test variant 1 (elast. suspension), Comparision

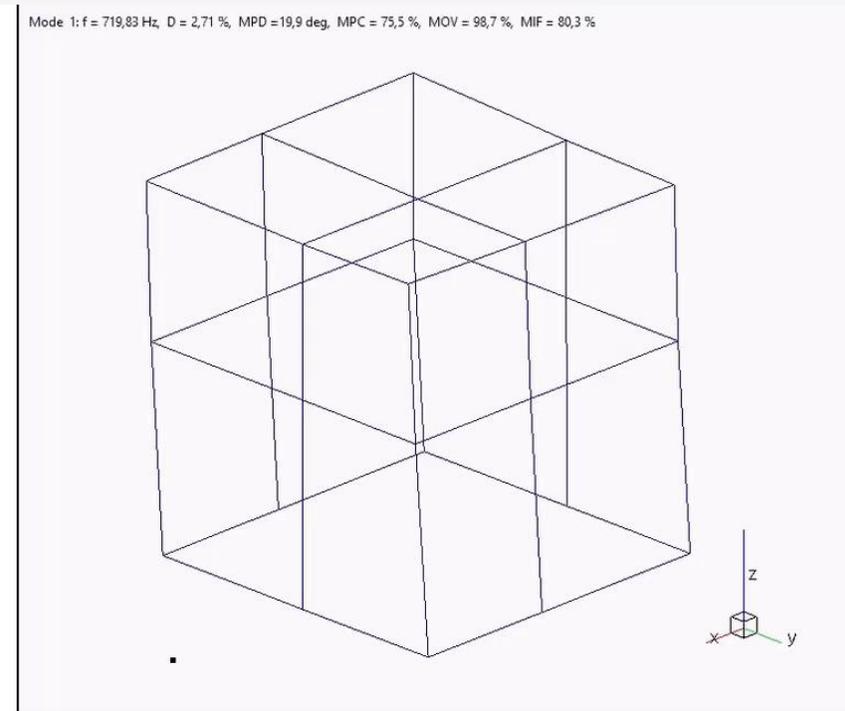
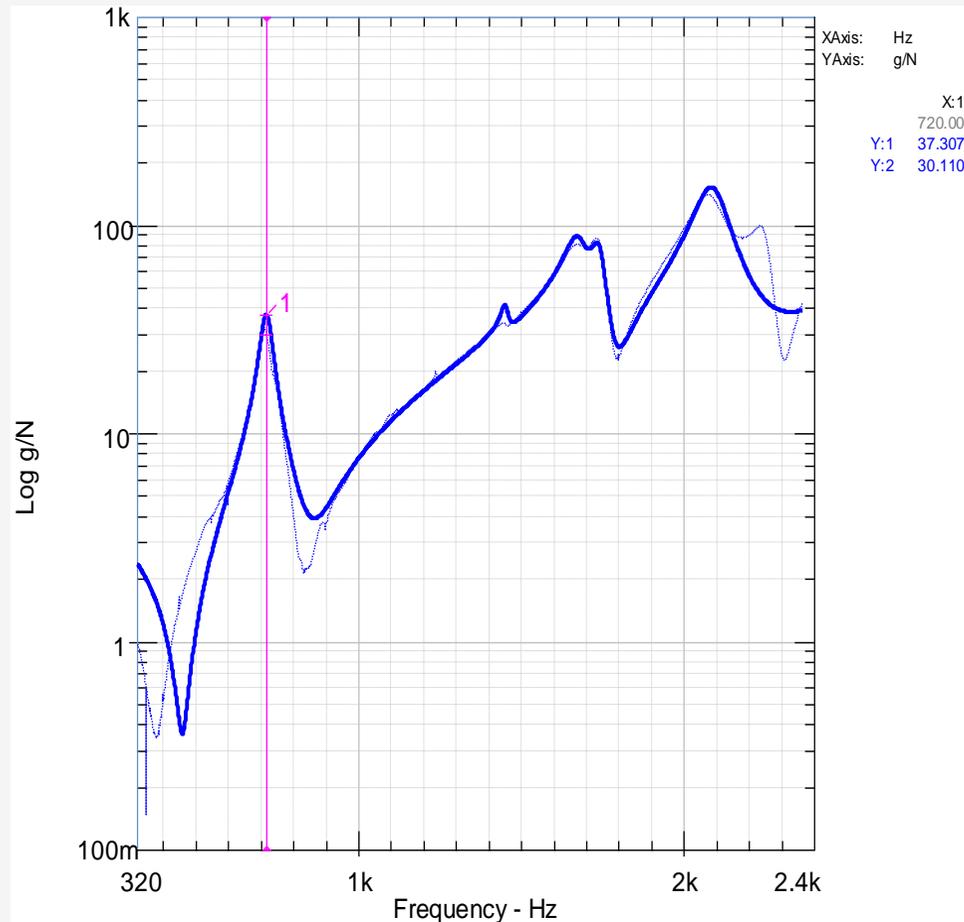
	Excitation +X			Excitation +Y			Excitation -Z		
	Natural freq.	Damping	MFI	Natural freq.	Damping	MFI	Natural freq.	Damping	MFI
1.Mode	1696,3 Hz	0,57%	91,2%	1696 Hz	0,58%	93,9%	1697,1 Hz	0,53%	71,8%
2.Mode	2155 Hz	0,29%	70,0%	---	---	---	2156,2 Hz	0,28%	82,6%
3.Mode	---	---	---	2277,3 Hz	0,23%	91,2%	2278,4 Hz	0,32%	82,8%
4.Mode	2520 Hz	0,38%	86,3%	2521,5 Hz	0,42%	80,2%	2518,3 Hz	0,47%	94,3%
5.Mode	2905 Hz	1,16%	88,8%	2912,6 Hz	0,23%	91,3%	---	---	---

Test results

- Test variant 2 (shaker armature), Impact in -Z

2. Mode (**not comparable with elastic suspension**):

Frequency: 720 Hz, Damping: 2,71%; Mode Indicator Function (MIF): **80,3%**

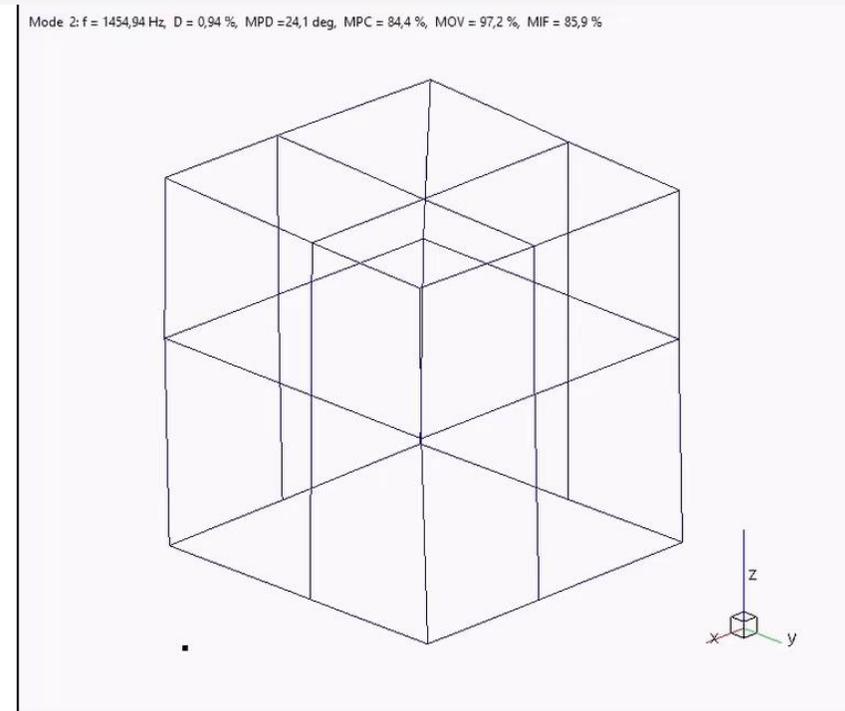
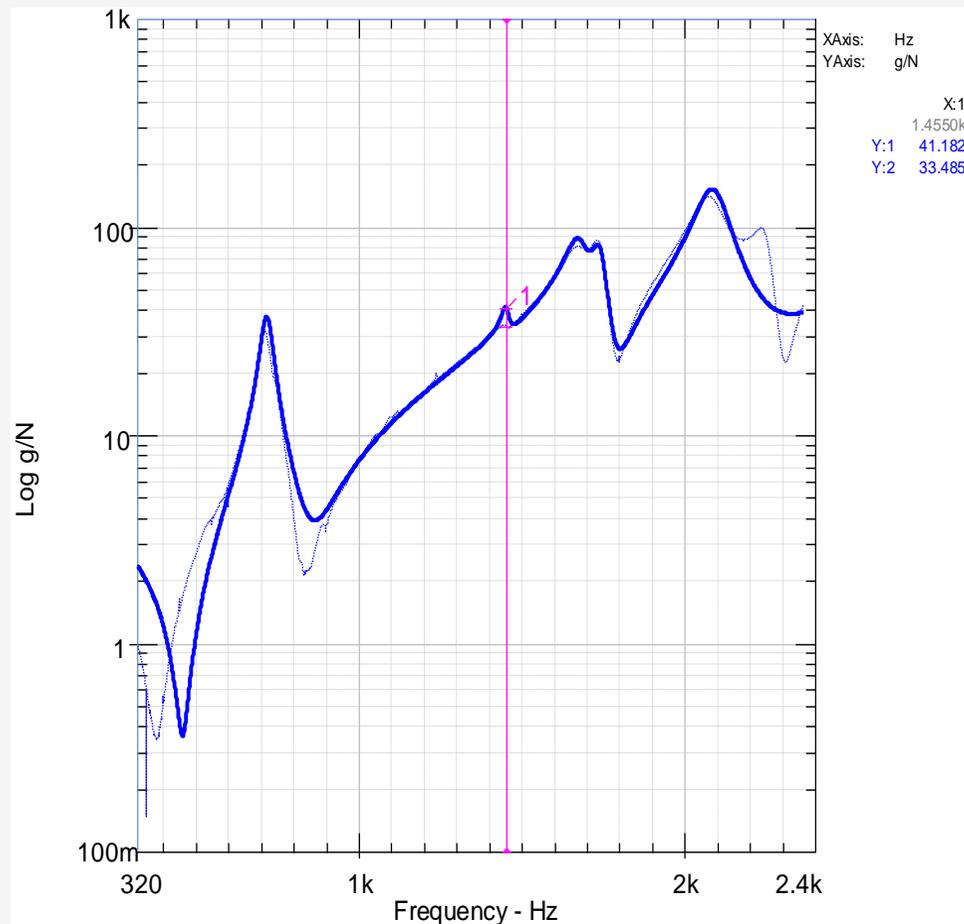


Test results

- Test variant 2 (shaker armature), Impact in -Z

4. Mode: Torsional mode (compare elastic suspension)

Frequency: 1455 Hz, Damping: 0,94%; Mode Indicator Function (MIF): **85,9%**

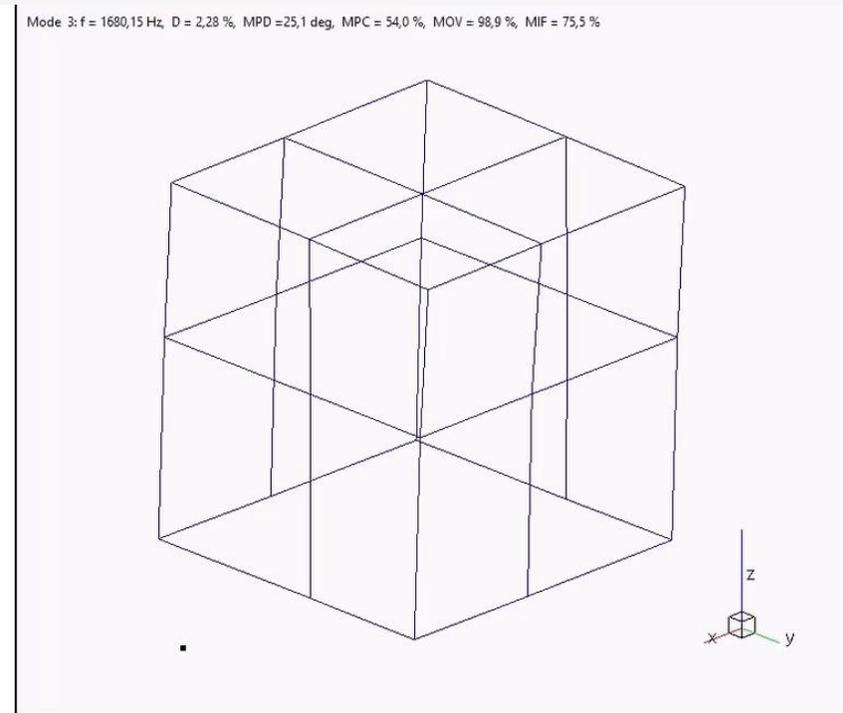
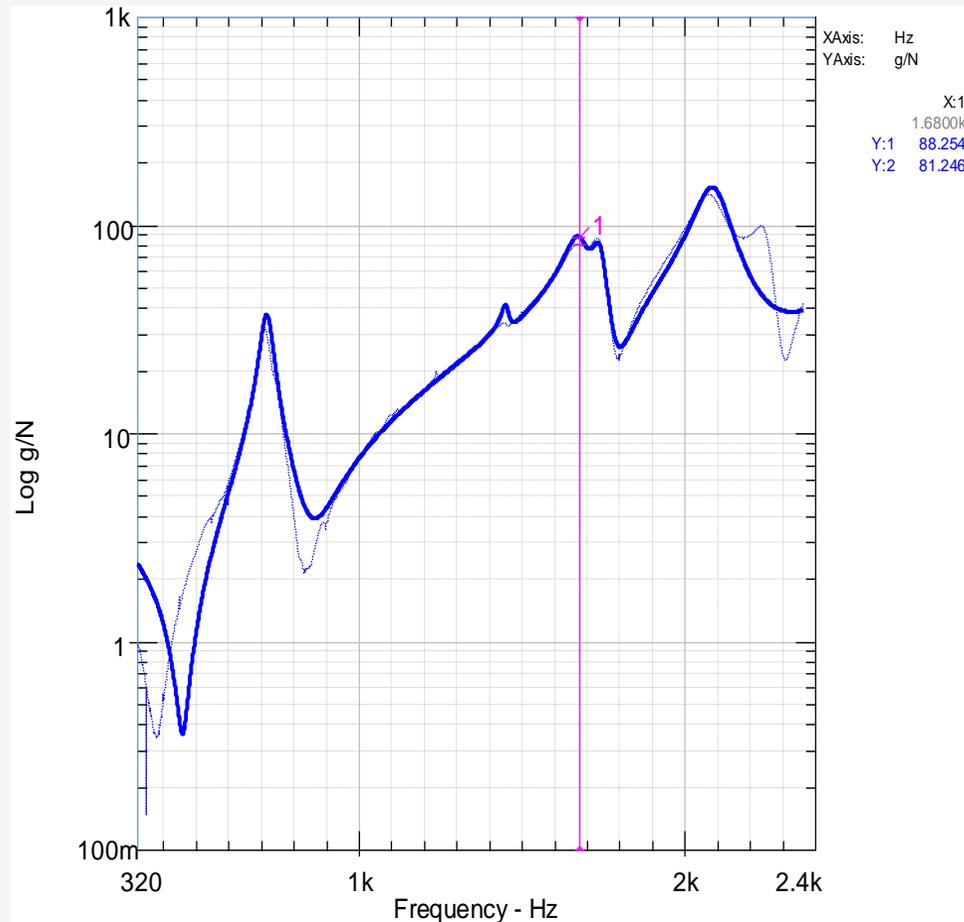


Test results

- Test variant 2 (shaker armature), Impact in -Z

5. Mode:

Frequency: 1680 Hz, Damping: 2,28%; Mode Indicator Function (MIF): **75,5%**

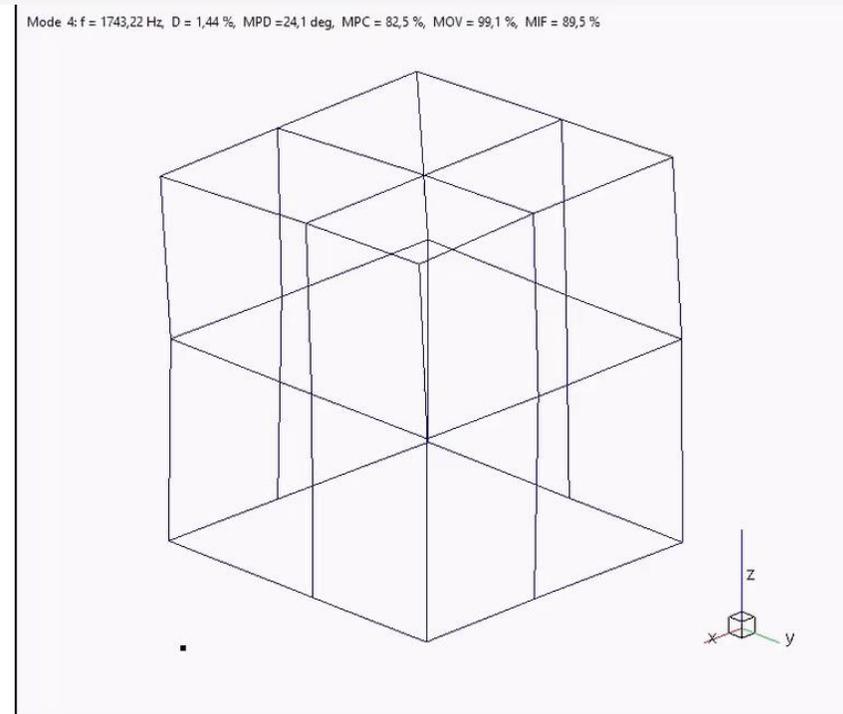
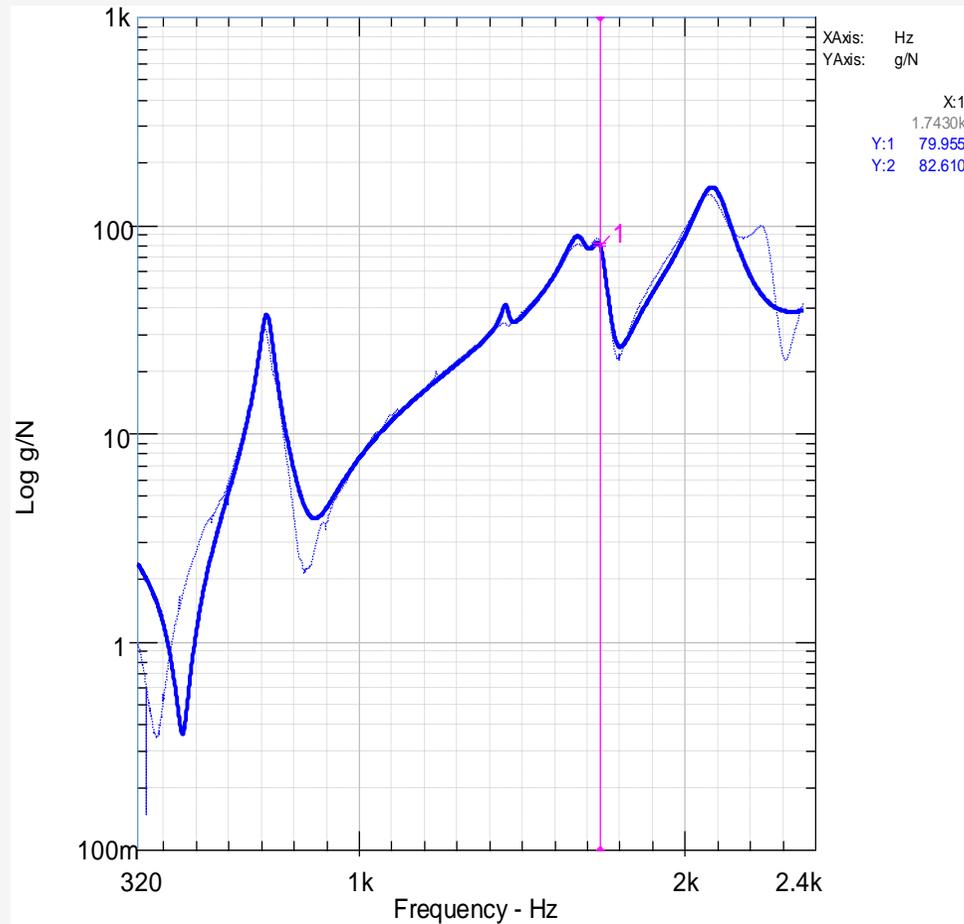


Test results

- Test variant 2 (shaker armature), Impact in -Z

6. Mode:

Frequency: 1745 Hz, Damping: 1,44%; Mode Indicator Function (MIF): **89,5%**

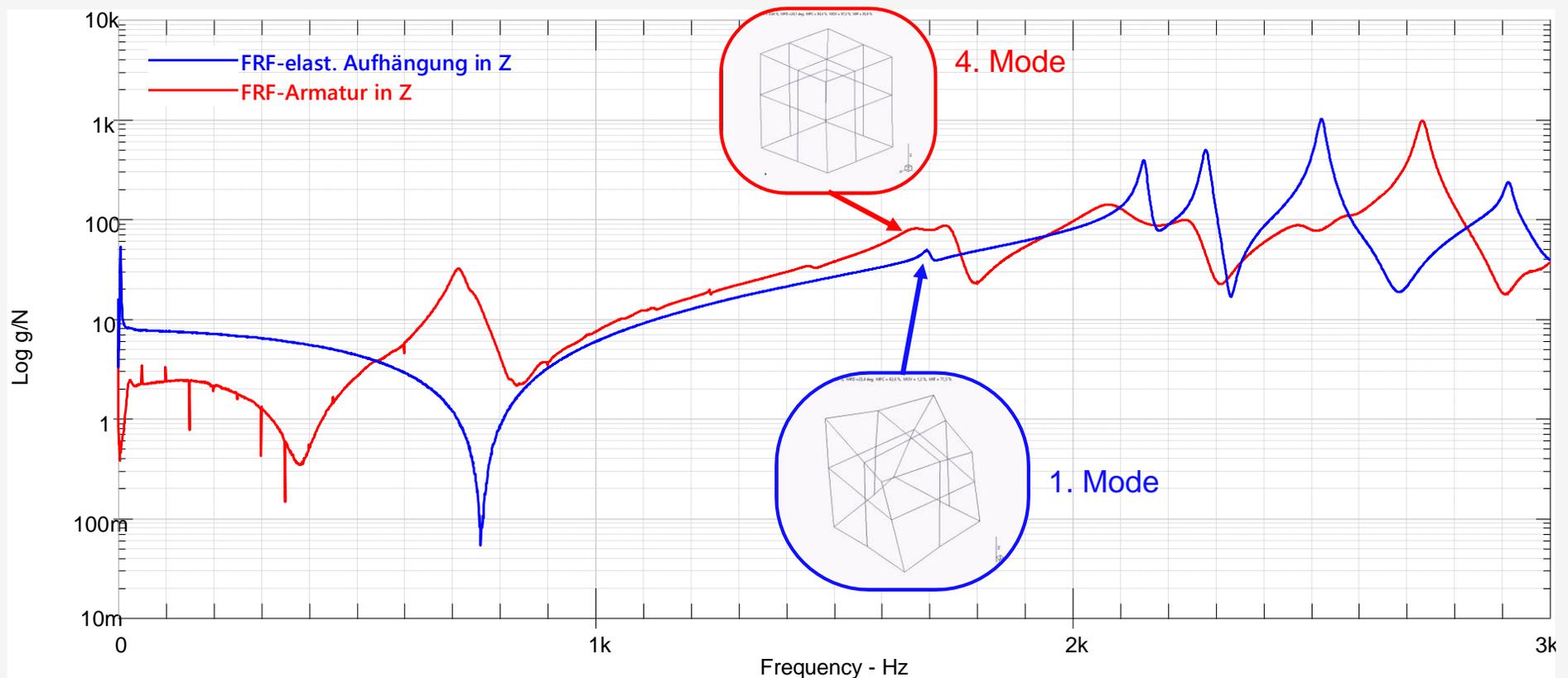


Test results

- FRF Test variant 1 vs. 2, Impact in -Z

Additional mass and coupling create additional constraints

- Increase of oscillating system mass (armature coil)
→ Natural frequencies move downwards
 - Additional mode shapes

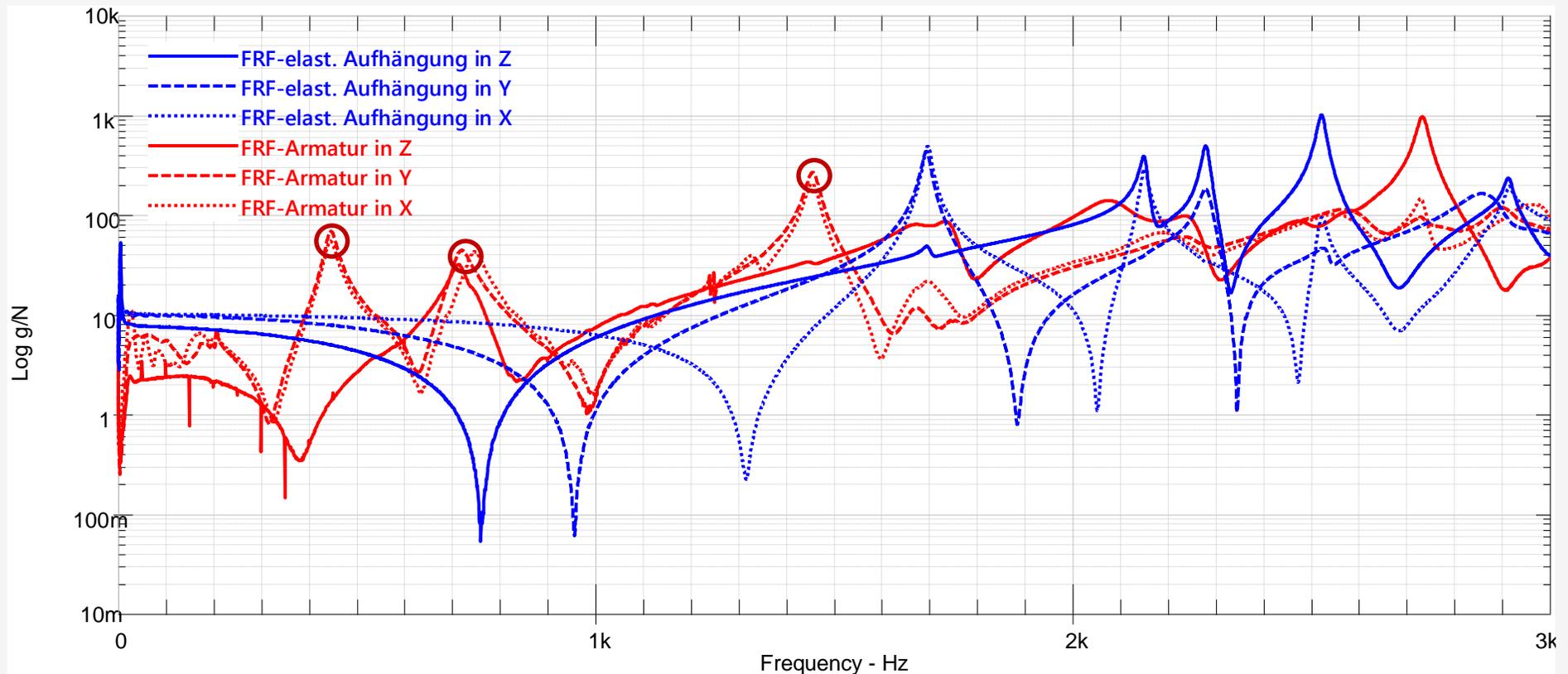


Test results

- FRF Test variant 1 vs. 2

Additional mass and coupling create additional constraints

- Increase of oscillating system mass (armature coil)
→ Natural frequencies move downwards
 - Additional mode shapes

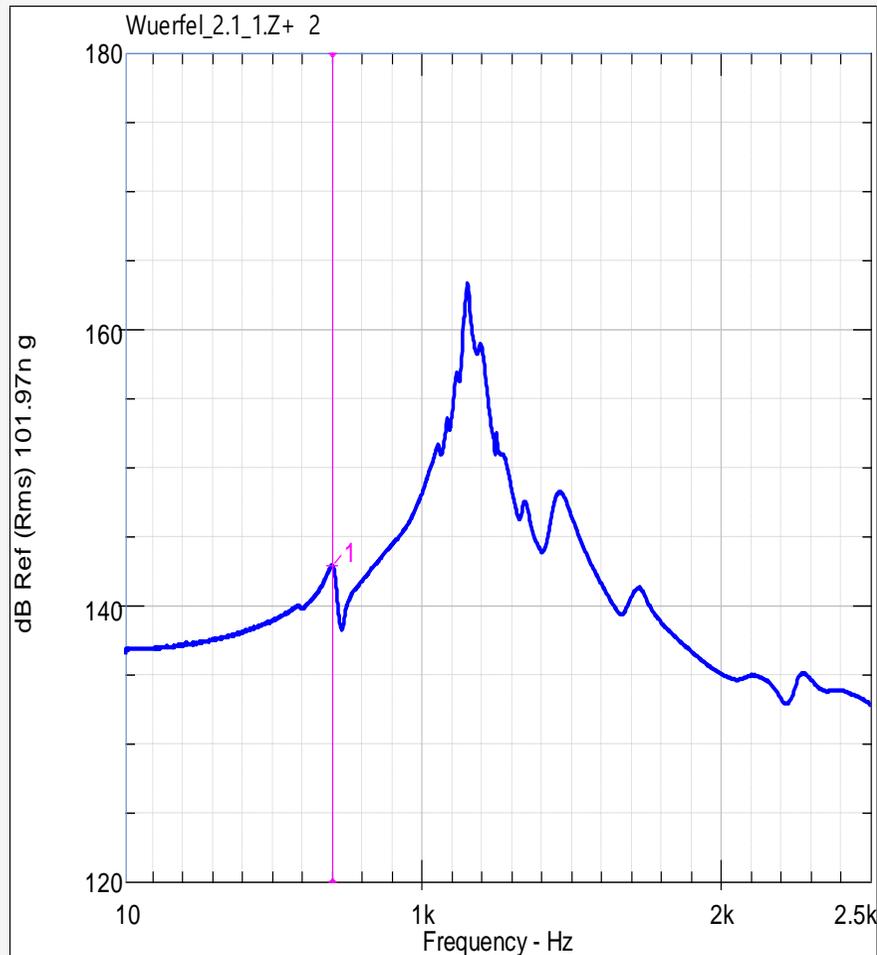


Test results

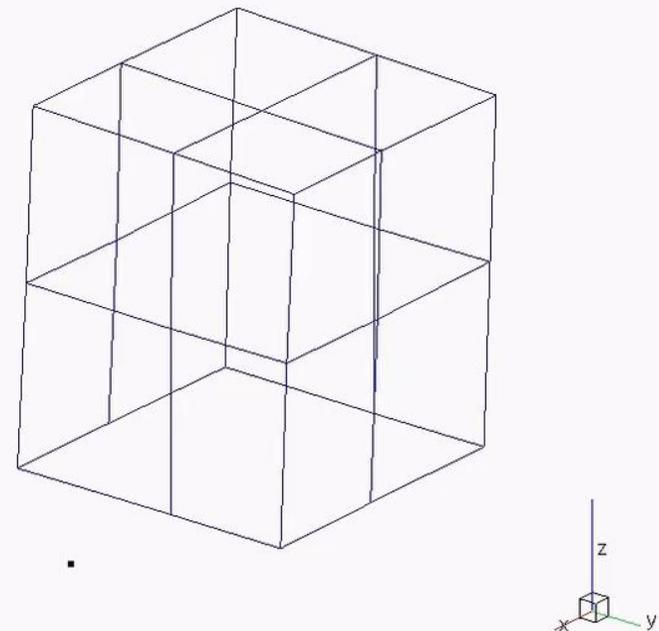
- Test variant 3 (shaker armature), Sine sweep in +Z

1. Operating deflection shape:

Frequency: 700 Hz, Damping: 2,7%; ODS (Operating Deflecting Shape)



Wuerfel_2
f = 701,04 Hz D = 2,70 % ODS [m]

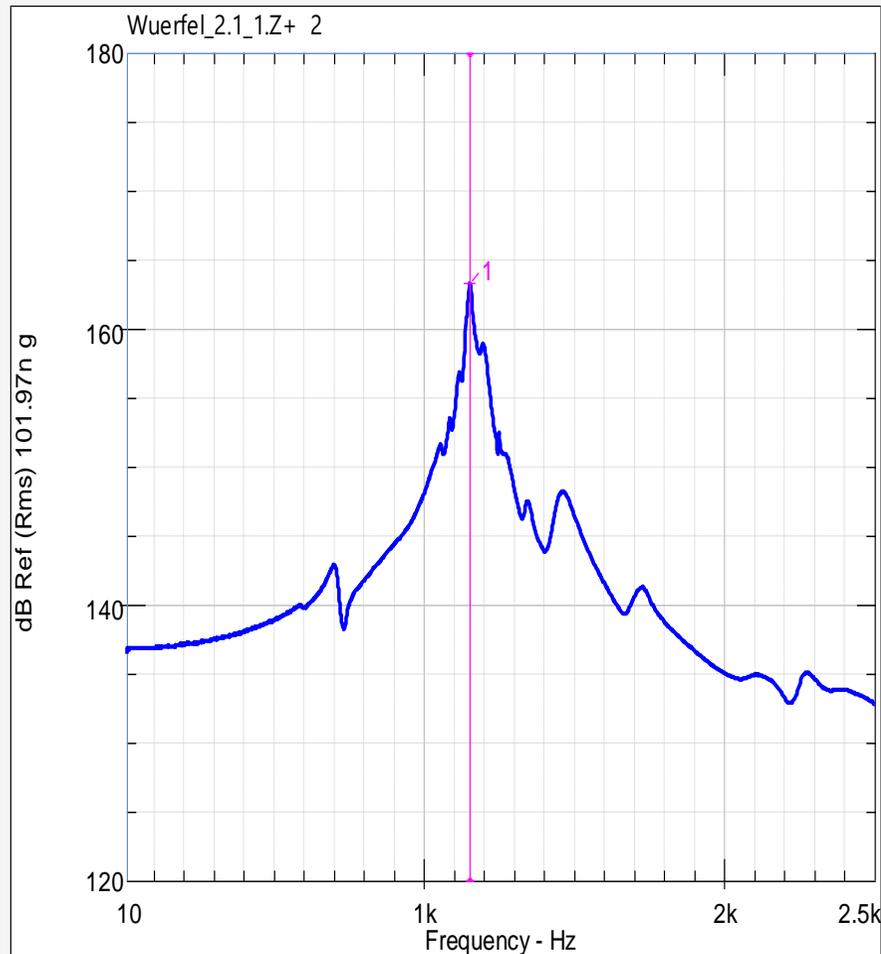


Test results

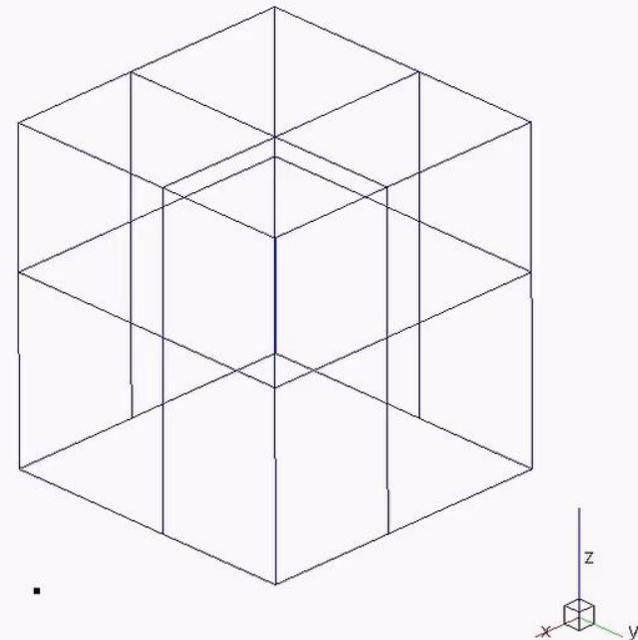
- Test variant 3 (shaker armature), Sine sweep in +Z

2. Operating deflection shape:

Frequency: 1150 Hz, Damping: 1,2%; ODS (Operating Deflecting Shape)



Wuerfel_2
f = 1149,87 Hz D = 0,00 % ODS [m]

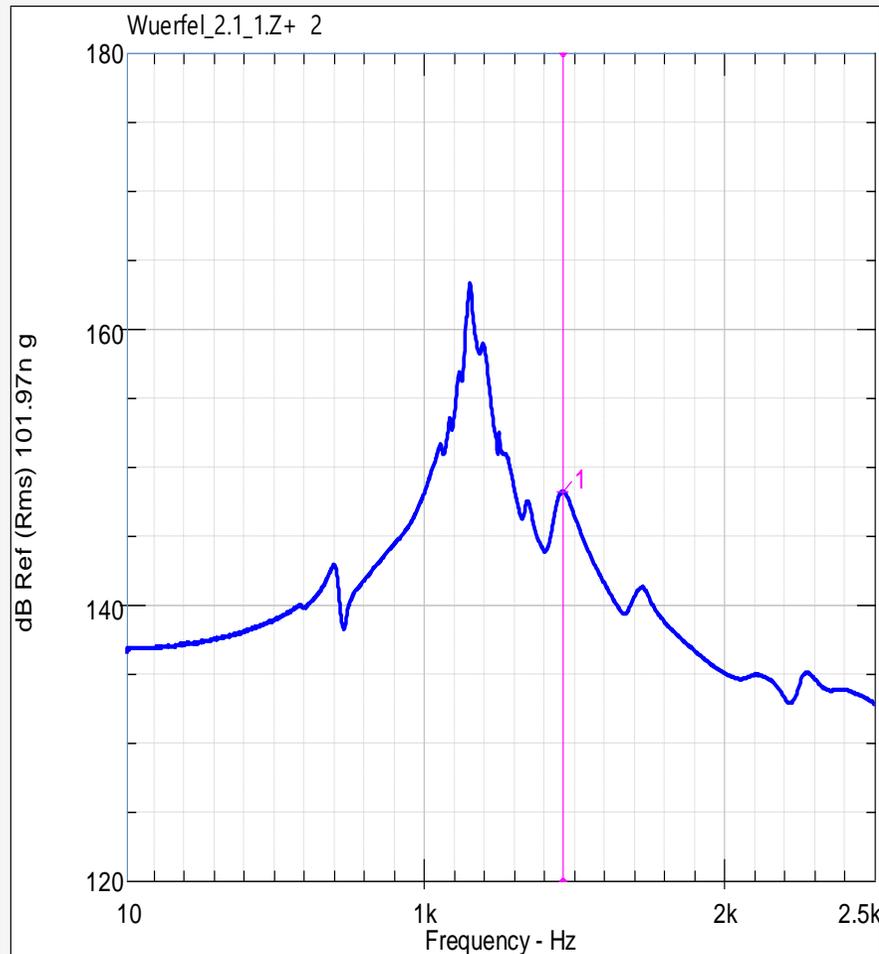


Test results

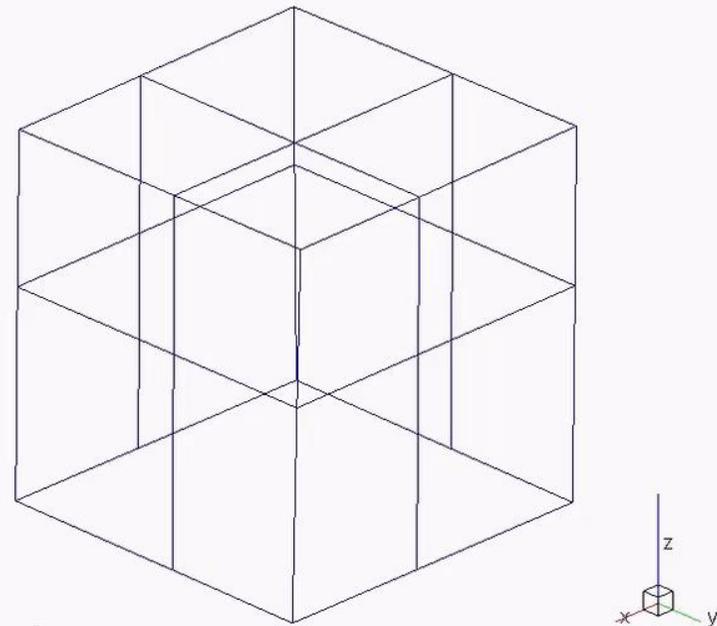
- Test variant 3 (shaker armature), Sine sweep in +Z

3. Operating deflection shape:

Frequency: 1460 Hz, Damping: 0,65%; ODS (Operating Deflecting Shape)



Wuerfel_2
f = 1461,77 Hz D = 0,65 % ODS [m]

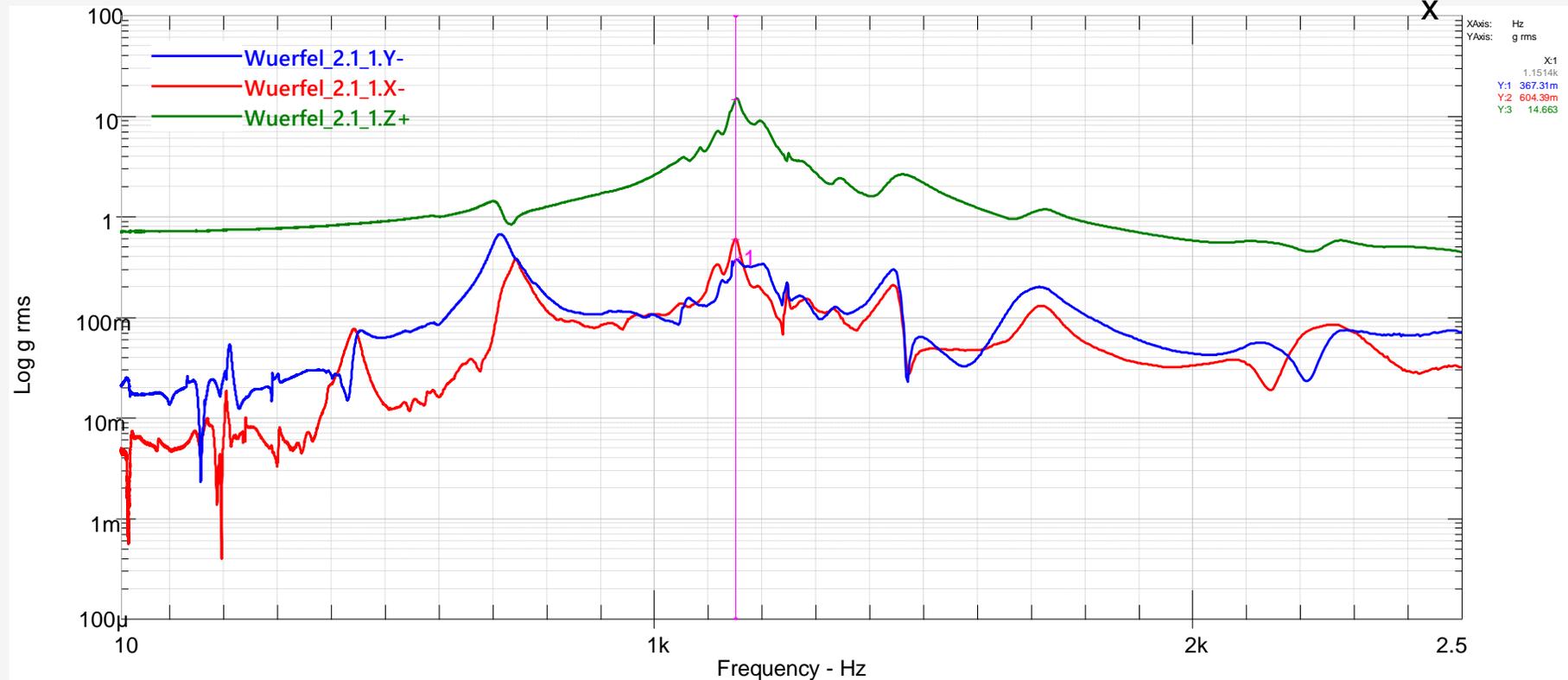
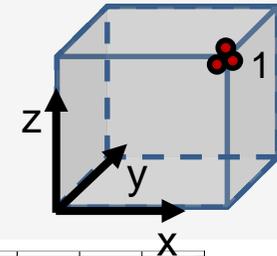


Test results

- Test variant 3 (shaker armature), Sine sweep in +Z

Response spectrum of measuring point 1 (x,y,z)

- Max. lateral acceleration in y: 0,7 g (rms), x: 0,6 g (rms)
- Max. vertical acceleration z: 15 g (rms) at 1155 Hz

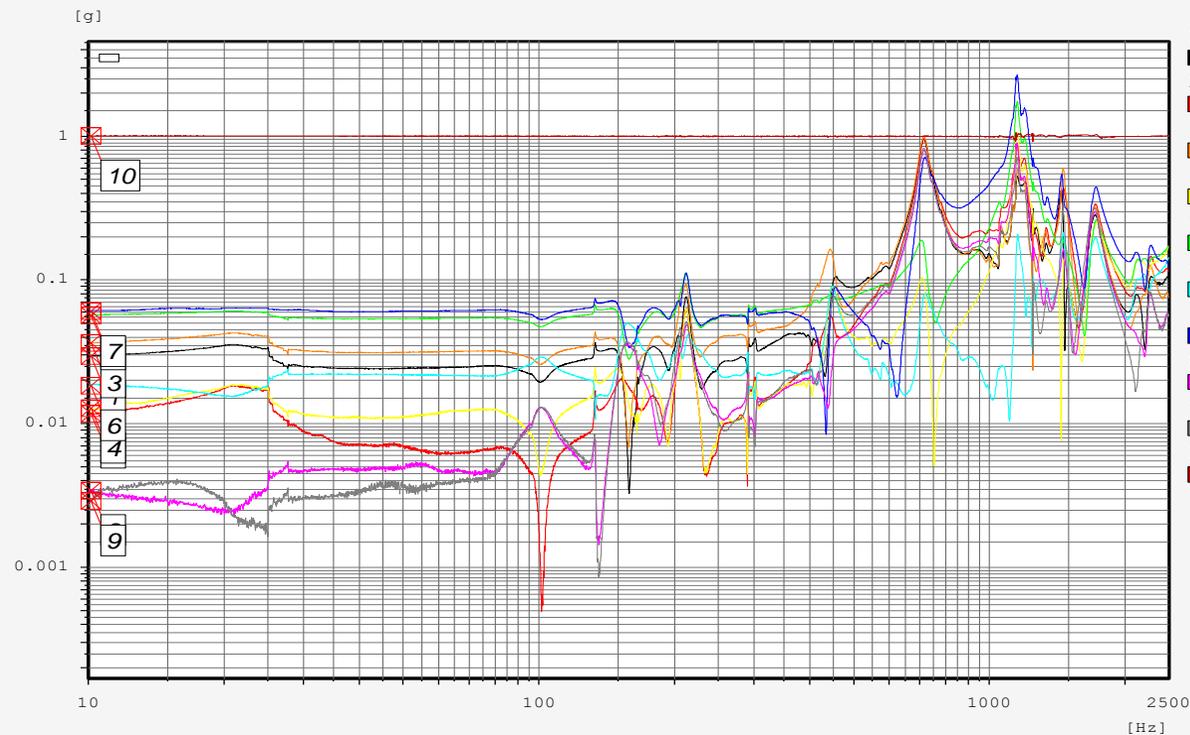


Test results

- Test variant 3 (shaker armature), Sine sweep in +Z

Spectra of measuring points in Y

Sine



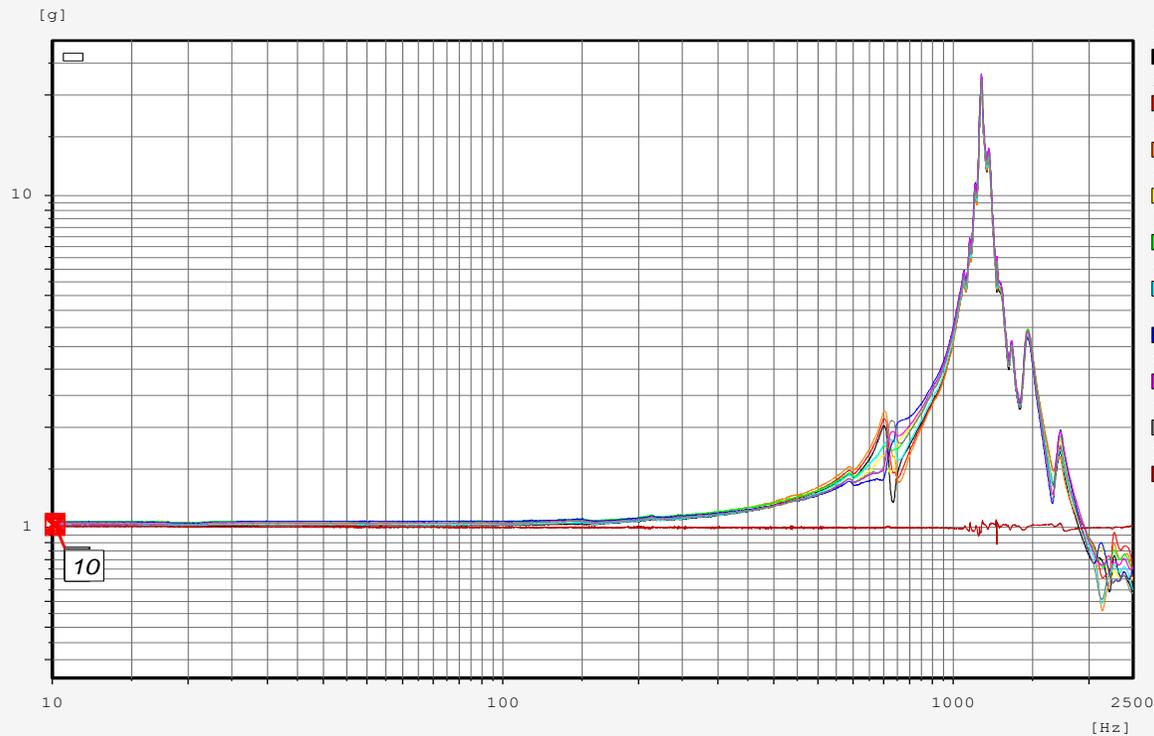
- 1. 002: Wuerfel_2.1_1.Y- [g] Filtered
- 2. 002: Wuerfel_2.1_2.Y- [g] Filtered
- 3. 002: Wuerfel_2.1_3.Y- [g] Filtered
- 4. 002: Wuerfel_2.1_4.Y- [g] Filtered
- 5. 002: Wuerfel_2.1_5.Y- [g] Filtered
- 6. 002: Wuerfel_2.1_6.Y- [g] Filtered
- 7. 002: Wuerfel_2.1_7.Y- [g] Filtered
- 8. 002: Wuerfel_2.1_8.Y- [g] Filtered
- 9. 002: Wuerfel_2.1_9.Y- [g] Filtered
- 10. 002: Würfel_2.0.Z+ [g] Filtered

Test results

- Test variant 3 (shaker armature), Sine sweep in +Z

Spectra of measuring points in Z

Sine

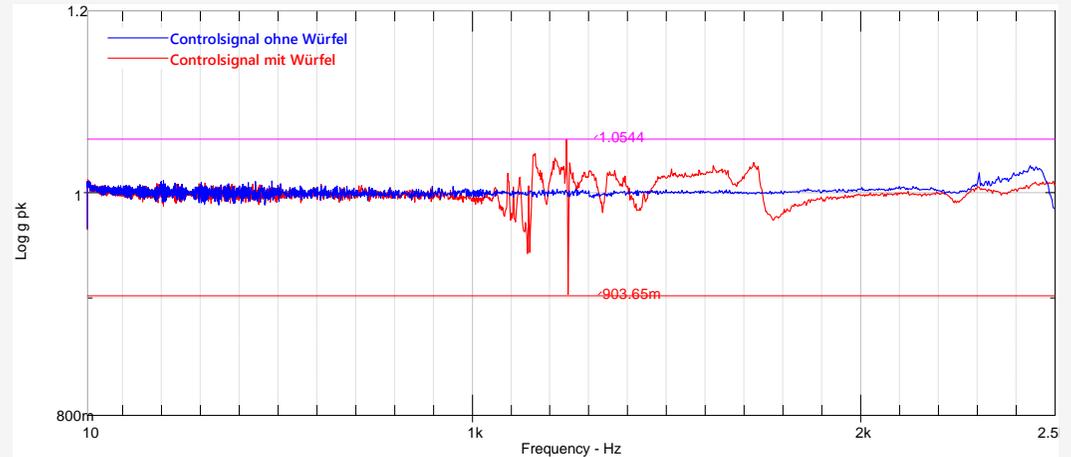


- 1. 002: Wuerfel_2.1_1.Z+ [g] Filtered
- 2. 002: Wuerfel_2.1_2.Z+ [g] Filtered
- 3. 002: Wuerfel_2.1_3.Z+ [g] Filtered
- 4. 002: Wuerfel_2.3_2.Z+ [g] Filtered
- 5. 002: Wuerfel_2.5_5.Z+ [g] Filtered
- 6. 002: Wuerfel_2.4_2.Z+ [g] Filtered
- 7. 002: Wuerfel_2.2_3.Z+ [g] Filtered
- 8. 002: Wuerfel_2.2_2.Z+ [g] Filtered
- 9. 002: Wuerfel_2.2_1.Z+ [g] Filtered
- 10. 002: Würfel_2.0.Z+ [g] Filtered

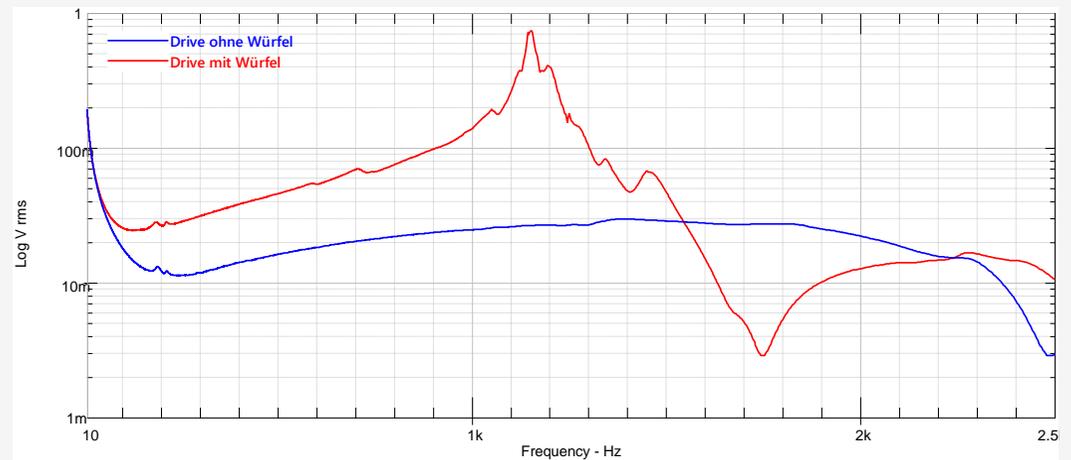
Test results

- Test variant 3 (shaker armature), Sine sweep in +Z

Control-Signal with and without cube



Drive-Signal with and without cube



- Investigation of the dynamic behavior of the test cube with and without coupling to the shake
- Identification of the influences by the coupling to the shaker
- Coupling extends the oscillating system (add. masses und stiffnesses)
 - Change of the modal parameters

- First natural frequency of the Cube at approx. 1700 Hz
- Influence of add. mass of the armature coil
 - Natural frequencies move downwards
 - Additional mode shapes
- First natural frequency of the cube + shaker armature at approx. 450 Hz
- First point of resonance (excitation in Z) at approx. 700 Hz
- Sweep excitation reveals strong resonance at 1150 Hz
 - Position of control channel on the cube (multi-point control)

Thank you for your attention !