

Tektronix and CN Rood Presents

The Standard Method for Measuring Switching Parameters



Agenda

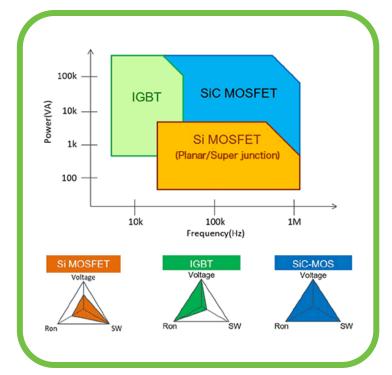


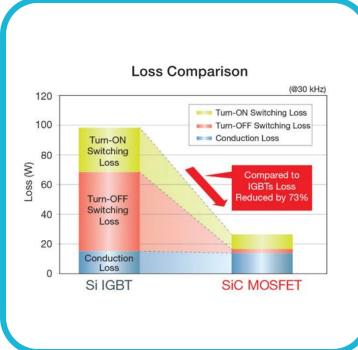
- Why Wide Bandgap (WBG) ?
- What is Double pulse test
- ☐ Principle and Key measurements
- Measurement Challenges
 - ☐ Gate driving Stimulus, Probing (Low /High Side), Deskew
- Questions

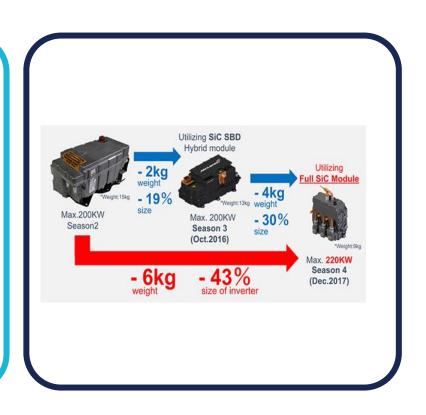


Why Wide Bandgap?









Higher Power Levels Faster Switching speeds

Lower Switching Losses

Smaller Form Factor



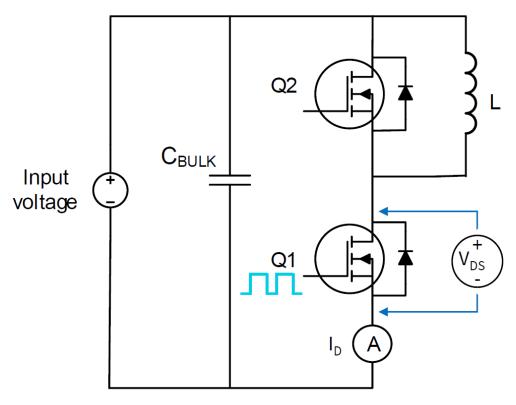


What is a Double Pulse Test?





DEFINITION



Double-Pulse Test Circuit

Evaluate and optimize the switching performance of power MOSFETs or IGBT Why?

- Gate drive optimization
- Calculating switching losses in the final design

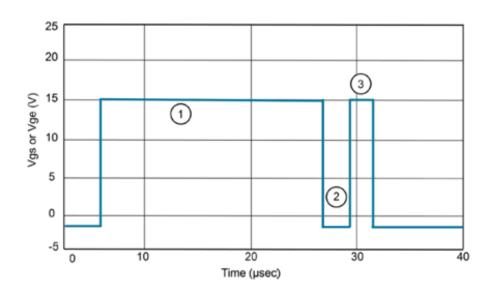
Dynamic performance evaluation over the full range of operating conditions

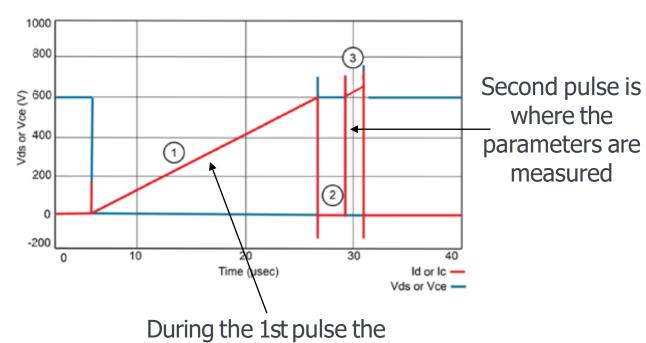
- Timing (Tdon, Tdoff, Trise, Tfall...)
- Amplitude (overshoot, ringing...)
- Speed (dI/dt, dV/dt ...)
- Switching energy (Eon, Eoff, Err...)



DEFINITION

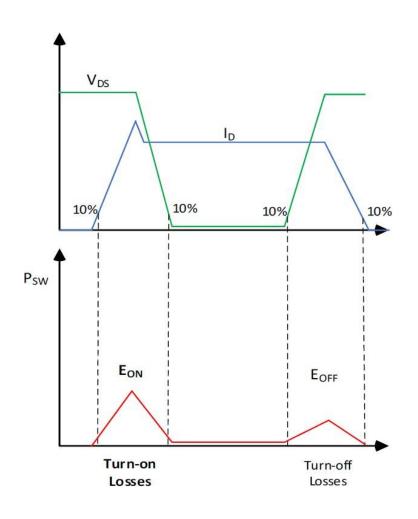
Q1 gate is driven with a controlled double pulse pattern, while Q2 is off







KEY MEASUREMENTS: EON, EOFF

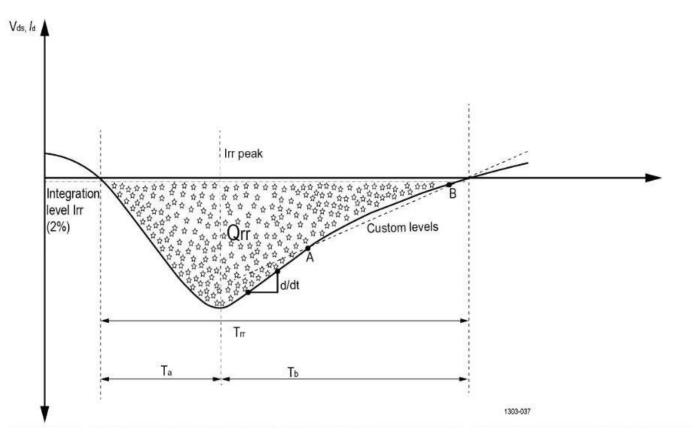


$$E_{on} = \int_{10\% Ids}^{10\% Vds} V_{DS} \times I_{DS}$$

$$E_{off} = \int_{10\% \, Vds}^{10\% \, Ids} V_{DS} \times I_{DS}$$



KEY MEASUREMENTS: REVERSE RECOVERY

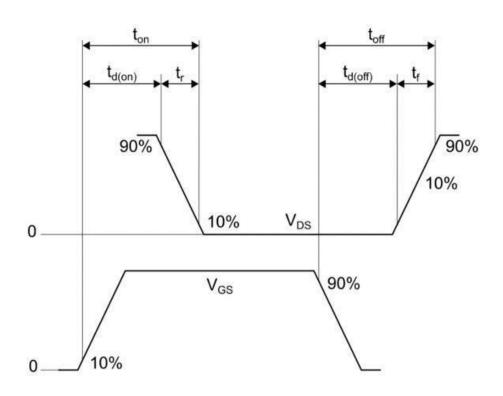


$$Qrr = \int_{t_0}^{t_0 + t_i} Irr x dt$$

$$Err = \int_{t_0}^{t_0+t_i} V_R \times Irr \times dt$$



KEY MEASUREMENTS: TIMING





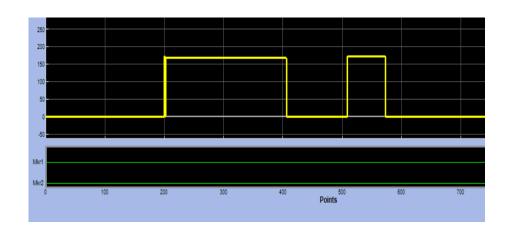
Measurement Challenges

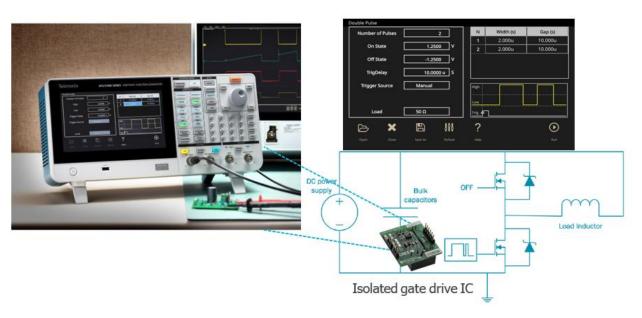
ASTRONIX CONFIDENTIAL AND ASSESSMENT AND ASSESSMENT AND ASSESSMENT AND ASSESSMENT ASSESSMENT





- Traditional function generator cannot control each pulse width individually
- Using PC to create arbitrary waveforms and load them onto the AFG is cumbersome and time consuming
- Using uC requires the user to write code. Off the shelf solutions lack flexibility







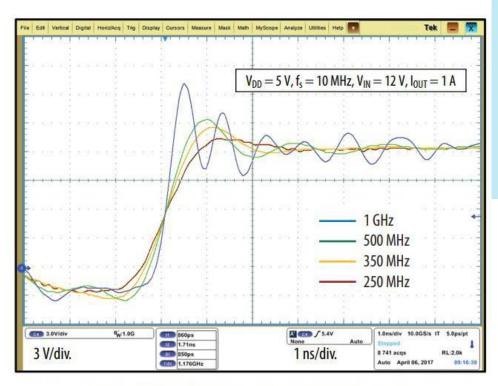








BANDWIDTH

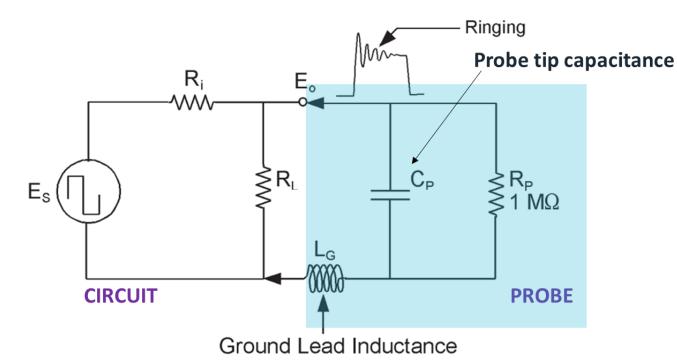


$$t_{r(probe)} = \frac{0.3 \dots 0.4}{BW} \qquad t_{r(measured)} = \sqrt{t_{r(signal)}^2 + t_{r(probe)}^2}$$

For reasonable accuracy, $t_{r(probe)} \approx 5 * t_{r(signal)}$

| Condition 30k to 80 kΩ resistor to GND | Тур | Unit |
|--|--|------|
| | | |
| CONTROL HOUSE SERVICE STATE OF THE SERVICE SER | 1.2 | V |
| RDHL = 30 kΩ | 0.8 | ns |
| RDHL = 80 kΩ | 3.4 | ns |
| RDLH = 30 kΩ | 0.8 | ns |
| RDLH = 80 kΩ | 3.2 | ns |
| | | |
| At min dead time | 8.4 | ns |
| 10%-90% | 1.0 | ns |
| 10%-90% with 1000 pF load | 2.5 | |
| 10%-90% | 1.0 | ns |
| 10%-90% with 1000 pF load | 1.8 | |
| 10%-90% | 0.9 | ns |
| 10%-90% with 1000 pF load | 2.5 | |
| 10%–90% | 0.9 | ns |
| 10%-90% with 1000 pF load | 1.8 | |
| | RDLH = 30 kΩ RDLH = 80 kΩ At min dead time 10%–90% 10%–90% with 1000 pF load 10%–90% 10%–90% with 1000 pF load 10%–90% 10%–90% with 1000 pF load | |

PARASITIC CAPACITANCE





- Decrease amplitude
- Change phase
- Slow down rise time tr=2.2*Rsource*Cp

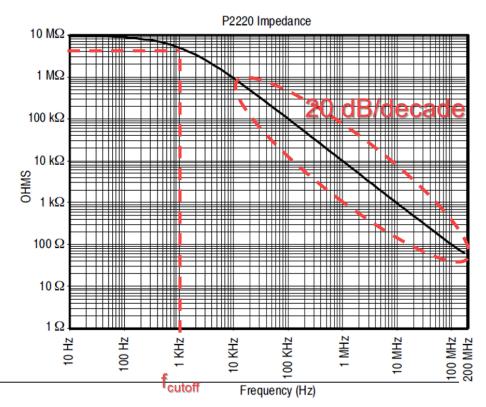
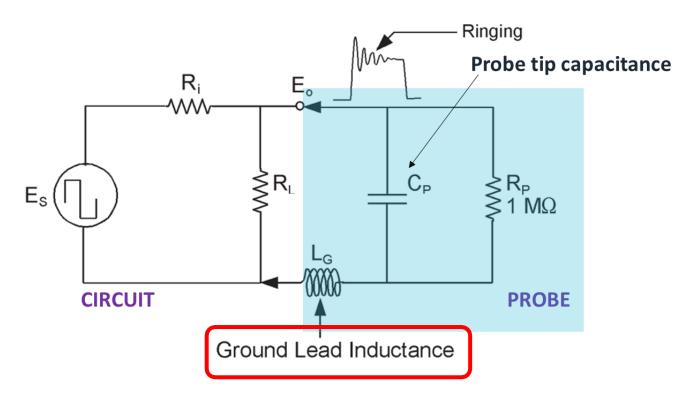




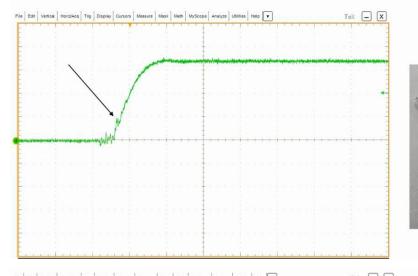
Figure 3: P2220 Input impedance

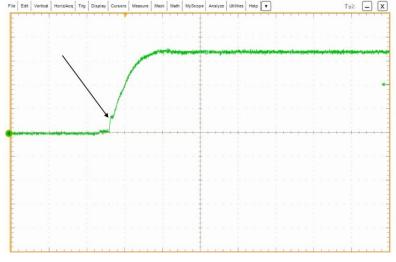
GROUND LEAD INDUCTANCE



Inductance +tip capacitance resonate =ringing







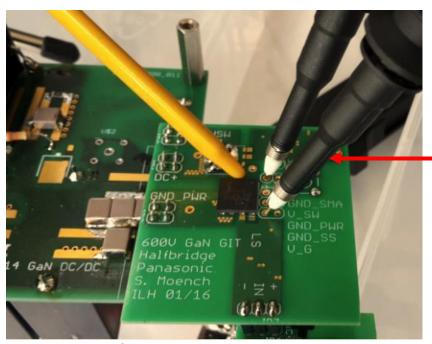




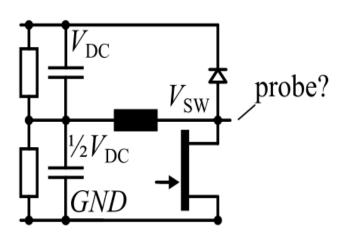


The importance of probing (low side)

Low Side Vds requires high bandwidth and high voltage capabilities



University of Stuttgart, Germany

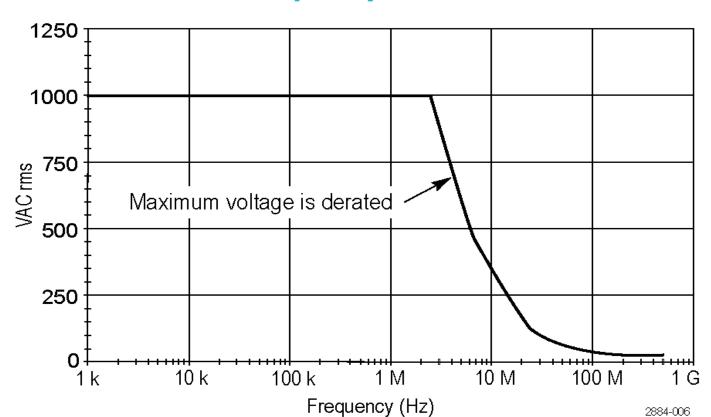








Beware of voltage derating vs frequency!





The importance of probing (High Side)

Differential probes are the preferred choice

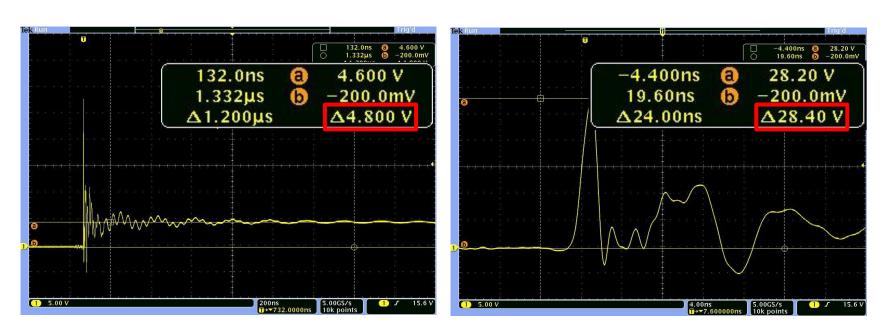


- Safety
- Reduce ground loop
- Common mode noise subtracted out of signal (CMRR)
 - Smaller input cap





Differential probes are expensive: Why not float the oscilloscope and use passive probes?



Bad signal fidelity (capacitive coupling) and unsafe

High side gate measurement comparison



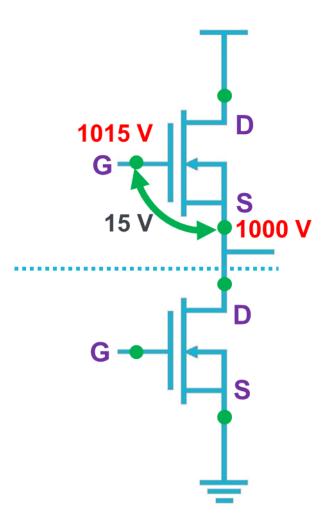




HIGH SIDE MEASUREMENTS CONSIDERATION

But high voltage differential probes have downsides

- High attenuation degrades signal to noise (High Side Vg)
- Radiated noise couples to the measurements through the leads
- Voltage derating vs frequency also applies
- CMRR is insufficient



CMRR

Bandwidth

CMRR DC

CMRR 1 MHz

CMRR 100 MHz

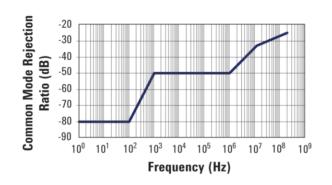
CMRR Full Bandwidth

Common Mode Error (1kV) @ DC

Common Mode Error (1kV) @1 MHz

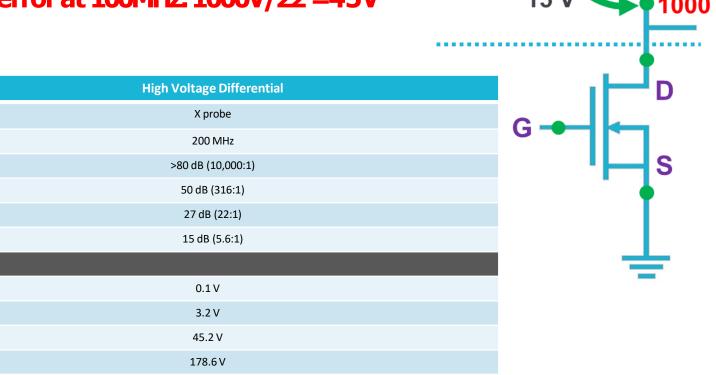
Common Mode Error (1kV) @100 MHz

Common Mode Error (1kV) @ Full BW



← Exemple of CMRR derating curve

CM error at 100MHz: 1000V/22 =45V



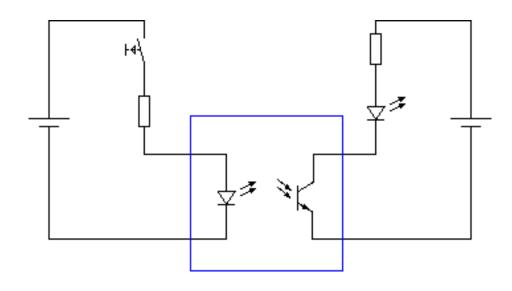
1015 V





INTRODUCTION TO ISOLATED PROBES

An isolated probe uses galvanic (optical) isolation to divorce the reference voltage of the probe from the reference voltage of the oscilloscope

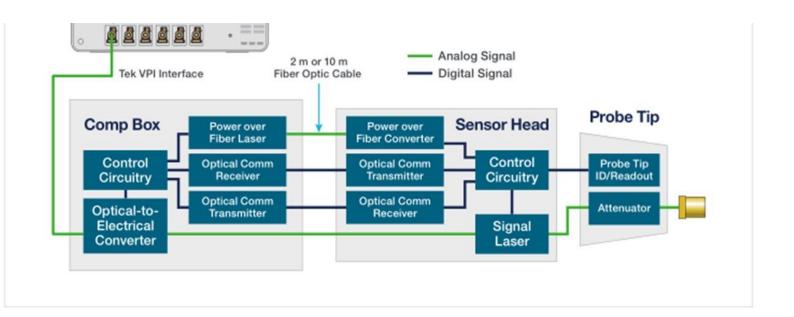


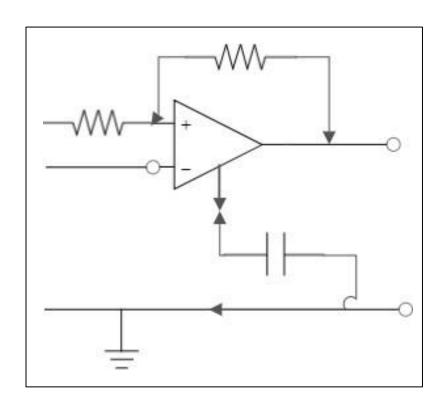
Advantages:

| | Isolated Probe |
|--------------------|---|
| EMI Susceptibility | Shielded Coaxial cable with common mode chokes; less coupling, less ringing |
| Cable Length | 2m fiber optic cable, 10m cable option |
| Safety | Complete galvanic isolation allows scope to sit outside PVC chamber |
| Ground Loops | Eliminates ground loops |
| Loading | No input +to ground loading |

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INTRODUCTION TO ISOLATED PROBES: NOTE ON ARCHITECTURE

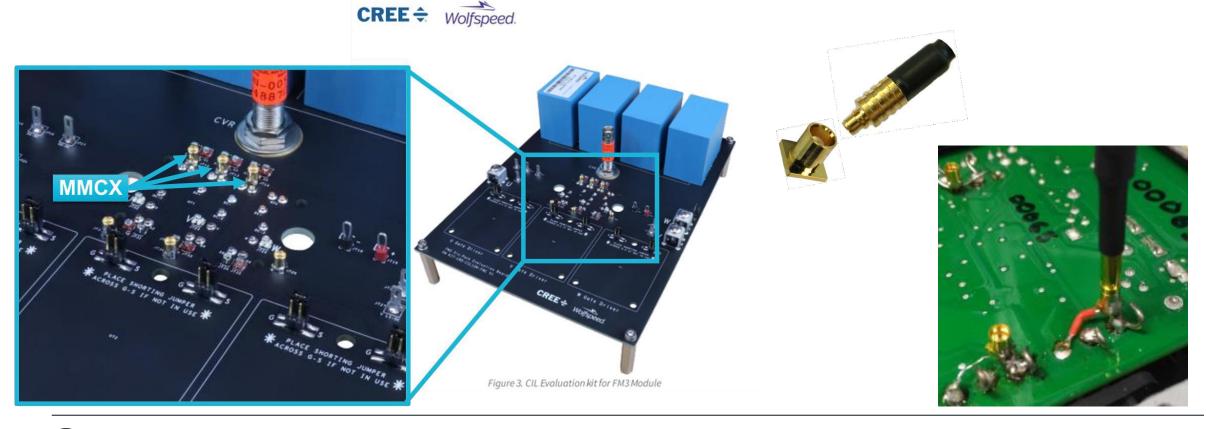






The importance of probing INTRODUCTION TO ISOLATED/Optical PROBES

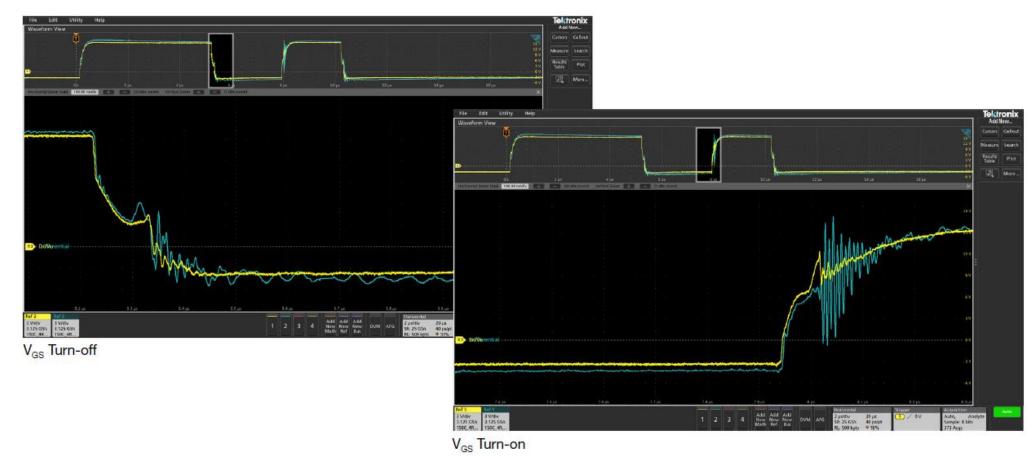
Planned test points (MMCX Connectors) → Best Performance MMCX connectors are small, **shielded**, inexpensive. They can be soldered onto unplanned test points.







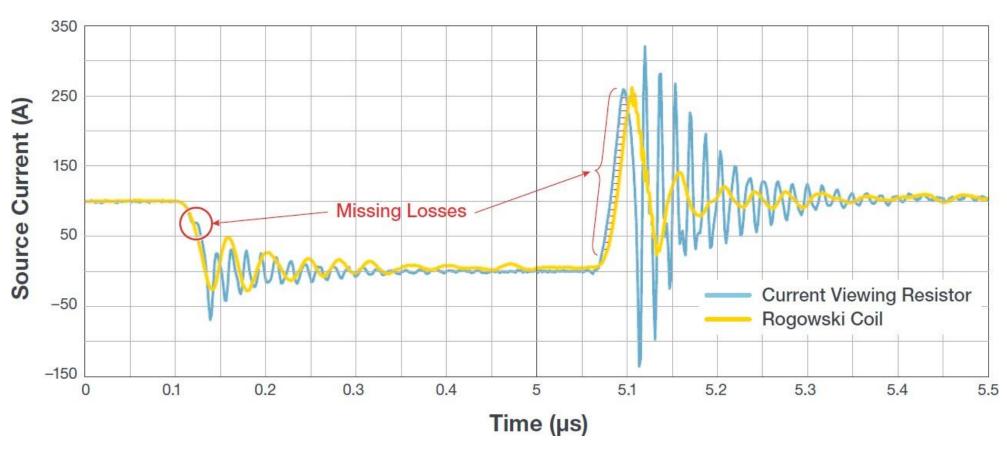
High Side Vgs example-Differential Probe (blue trace) vs. Optically Isolated Probe (yellow trace).





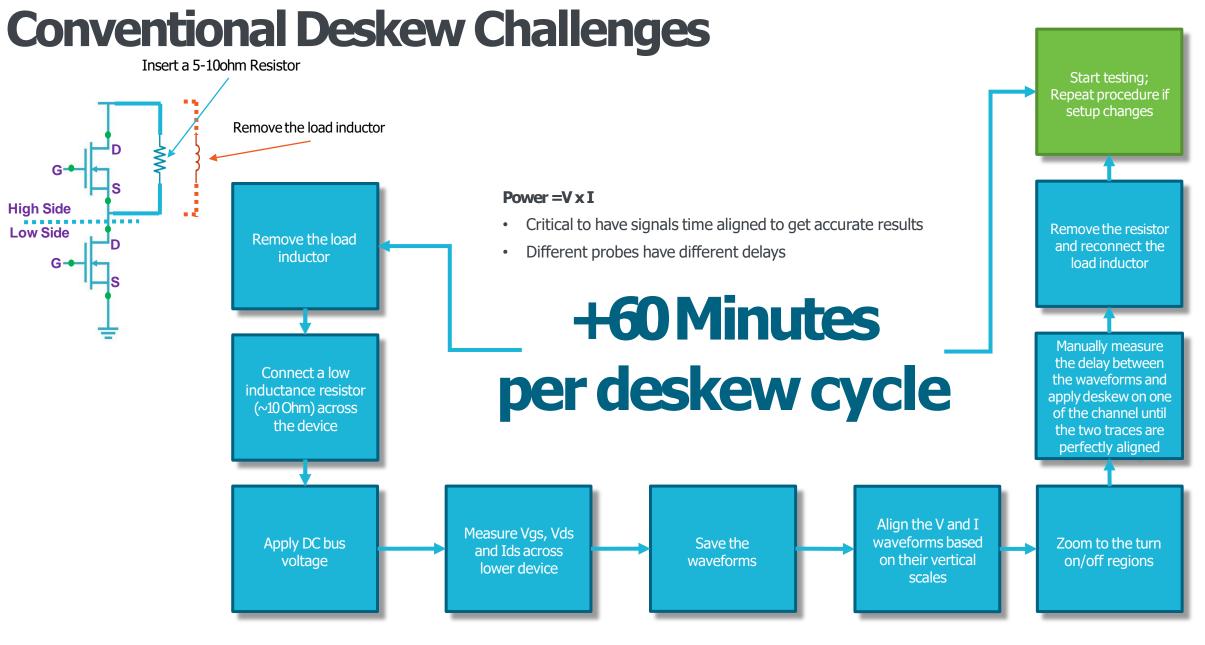


CURRENT MEASUREMENTS



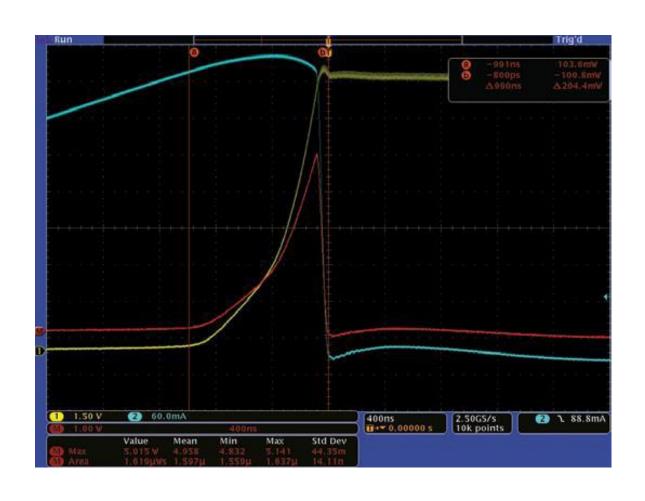
CVR vs Rogowski Current Probe, CAB011M12FM3 (TJ = 150°C, RG = $1~\Omega$), VDS = 600~V, IS = 100~A).





Deskew





Switching loss **Mean power =4.958 W**



DESKEW

Mean power =5.239 W

5.6% error w/o deskew





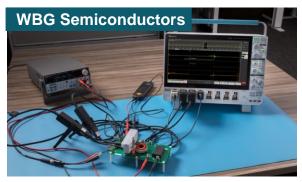


Complete Wide Bandgap Validation





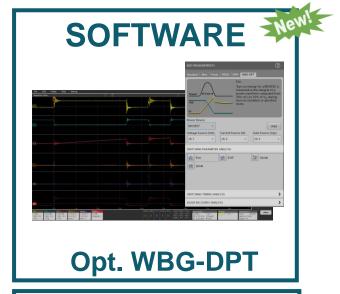












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Thank you ..



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